# **Geotechnical Investigation and Dam Stability Analysis**



Project: 1075 Horseshoe Bend Road, Torquay Report No: AGTE17463

Adelaide, Ballarat, Brisbane, Dingley Village, Warrnambool



**Prepared for:** 

The Dunes, Torquay

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# 1. Introduction

Australian Geotechnical Testing (AGT) was engaged by The Dunes, Torquay to undertake a Geotechnical investigation and Dam Safety Assessment for the existing Dam at 1075 Horseshoe Bend Road, Torquay.

Specifically, the Dam Safety Assessment was required to due to the following:

- An inspection of the above dam was made by officers from Southern Rural Water on 5th October 2017.
- In accordance with the Water Act 1989 & government policies, your dam is regarded as
  potentially hazardous. Due to their size and dimensions hazardous dams could cause
  significant damage to public and private property, the environment, and pose a threat to
  personal safety if they were to fail. For these reasons the Ministerial Policies require owners
  of these dams to have the integrity of the dam assessed by an engineer every 5 years, and
  develop a maintenance and surveillance plan. As the corporation responsible for licensing
  farm dams in your area, Southern Rural Water is required to implement this requirement for
  all dams in the above criteria.

From this Dam Safety Assessment Report that includes:

• Integrity of the dam structure and design, and advise any remedial action required.

This Geotechnical Investigation and Dam Safety Assessment report presents a summary of the subsurface conditions encountered, discusses the results and provides recommendations for remedial action for the dam.

## 2. Site Description

### 2.1 Locality

The site location is located along Horse Blend Road adjacent to the Golf Coarse and within agricultural farming.

#### Figure 2.1





### 2.2 Topography

The topography of the site was relative level with a maximum slope within the vicinity of the dam of a slope of 1:140.

### 2.3 Regional Geology

Geological Survey of Victoria maps (1:63,360) and information published by the Department of Primary Industries on the GeoVic on-line geological mapping site (1:250,000) shows the site is underlain by:

• Quaternary Sandy clay and clayey quartz sand

In general, the anticipated subsurface conditions have been encountered during this site investigation and are considered to be consistent with the geological map.

## 3. Site Investigation

The field investigation was undertaken on 8-9/12/2017 which involved a site inspection and drilling of 8 boreholes to a depth of up to 6.5-9.0m or refusal. This geotechnical investigation was aimed at providing geotechnical subsurface profile and design parameters to assist with the development of the assessment of the dam stability. Representative sample was collected for laboratory testing.

Engineering Logs of the boreholes are presented as Appendix B.

#### **3.1** Boreholes Profile

Table 3.1 presents a summary of subsurface profile for the 8 boreholes.

Table 3.1 – Summary of Subsurface Profile

Matarial	Depth (m)												
Material	BH 1	BH 2	BH3	BH4									
Fill, Sandy Clay	0-7.05	0-6.1	0-6.1	0-7.5									
Sandy CLAY	7.05-8.0	6.1-6.5	6.1-6.5	7.5-8.5									
Total Depth	8.0	6.5	6.5	8.5									



Matarial	Depth (m)													
Material	BH5	BH6	BH7	BH8										
Fill, Sandy Clay	0-7.5	0-6.8	0-2.9	0-7.1										
FILL, Clayey Sand			2.9-3.1											
Fill, Sandy Clay			3.1-6.5											
FILL, Clayey Sand			6.5-8.0											
Sandy CLAY	7.5-8.5	6.8-7.5	8.0-9.0	7.1-7.5										
Total Depth	8.5	7.5	9.0	7.5										

#### 3.2 Groundwater

Groundwater was not encountered at any exploratory location during the on-site field investigation.

### 4. Dam

### 4.1 Type of Dam (Tank)

The dam is a rectangular tank with the wall raised above the natural surface preventing any surface runoff entering the dam. The dam is a storage tank that obtains its water from pumping water from the Black Rock treatment plant. Minimal water is obtained from rainfall over the dam.

#### 4.2 Runoff Estimates

As the dam is a tank design that has been raised above the surrounding area, there will be no runoff into the dam.

#### 4.3 Catchment Area

The only catchment area is the actual dam itself and the surface area of the extents of the dam walls.

#### 4.4 Estimation of Flood Flows

During flooding rains the only impact will be the rain itself. The maximum rainfall according to the Burau of Meteorology Website for the Torquay Golf Club weather station for a day was 90mm in February 2002. With a minimum freeboard of 1.0m, there would be no risk of flooding of the neighbouring properties due to overtopping of the dam.

#### 4.5 Water Requirements

The water requirements are for the watering of the agricultural land of the property.

#### 4.6 Homogenous Dam

It is believed that the dam has a homogeneous wall. Within the previous 6 months some additional Sandy Clay material has material been added widening the crest of the dam wall. This material has



been well compacted. On the outer edge of the walls their has been some loose material placed. The thickness of this loose material has been estimated at 0.2-0.5m. This loose material has no impact as the structural integrity of the dam wall.

#### 4.7 Dam Design

The dimension of the dam is  $250 \times 120$  m with a surface area of the water of 30,000 m<sup>2</sup>. The dam height of 7.81 m.

It has been assumed that wall of the dam continues at the same slope of the observed wall to a depth of 3m below ground levels outside the dam. It is believed that after the floor of the dam was stripped of all unsuitable material (No unsuitable material was found in the geotechnical investigation of the walls of the dam., the Sandy CLAY was excavated to be used for the walls of the dam.

The estimated volume of the dam at its current water level is 90ML. The potential volume of dam would be approximately 300ML 1m below the crest.

#### 4.8 Inlet Pipe

An inlet pipe was observed in front of the western embankment. This water is sourced from the Black Rock Treatment Plant which transfers treated water into the dam. The flow of water can be stopped at any time.

#### 4.9 Outlet Pipe

At the eastern extent of the dam the outlet pipes transfer the dam water throughout the pump to the agricultural site.

#### 4.10 Spillway

No spillway was observed and due to the type of dam is not required.

#### 4.11 Field Assessment

A field assessment was undertaken on the 8-9<sup>th</sup> November 2017 for the purpose of assessing the dam in relation to the structural integrity. The walkover survey viewed the entire dam are and surrounding property. Photos of the site indicating the site area and dam were taken to assist in the assessment (refer to Appendix F)

#### 4.11.1 Seepage/Leakage

No evidence of seepage or leakage of the dam was observed.

#### 4.11.2 Erosion

No evidence of erosion of the dam was observed.

#### 4.11.3 Deformation/Movement

No evidence of deformation or movement of the dam was observed.

#### 4.11.4 Shrinkage/Cracking

Minor shrinkage and cracking was observed in the surface material along the crest of the wall and the outer wall of the dam. This cracking was predominantly observed in the recent material that was placed.



#### 4.11.5 Shrinkage/Cracking

Minor shrinkage and cracking was observed in the surface material along the crest of the wall and the outer wall of the dam. This cracking was predominantly observed in the recent material that was placed.

#### 4.11.6 Trees

Trees were observed along the inner wall of the dam (Refer to Appendix B). These trees are estimated to be on the wall for at least 15 years within no detrimental effect on the structural integrity of the dam wall. Due to the width of the dam, the material type and compaction of the dam it is believed that these trees will continue to have no structural detrimental effect on the dam. Large trees were observed in the neighbouring property along the western wall. Due to the distance from the dam, the material type and compaction of the dam it is believed that these trees will also continue to have no structural detrimental effect on the dam.

## 5. Field and Laboratory Testing

Field testing comprised Standard Penetration Tests (SPT) tests at boreholes at various depths. Laboratory testing comprised 35 moisture content tests, 7 sieve analyses, 7 Atterberg Limits tests, 5 Permeability Tests and 10 Emerson Tests.

A summary of the results obtained is shown within Table 5.1 below. NATA Test Certificates for each of the laboratory tests are attached as Appendix C.



#### Table 5.1

	(m)	(mr			(%)	( <sub>6-</sub>		nsity				(%)		(%) Pa	assing	
Location	Layer Depth From (m)	Layer Depth To (mm)	Material	USC (AS1726)	Moisture Content (%)	Permeability (x10 <sup>-9</sup> )	Emerson	Maximum Dry Density	OMC	Liquid Limit	Plasticity Index	Linear Shrinkage (%)	0.075mm	0.425mm	2.36mm	19.0mm
	1.0		Sandy Clay		19.1											
	2.0		Sandy Clay		18.7											
	3.0		Sandy Clay		25.4											
	3.0	4.0	Sandy CLAY	СН						58	36	12.5	57	82	93	100
BH1	4.0		Sandy Clay				4									
DIT	5.0		Sandy CLAY		31.8	2x10 <sup>-10</sup>										
	6.0		Sandy Clay		22.7											
	6.0	7.0	Sandy CLAY	CI	20.2					39	21	10.0	60	83	94	100
	7.0		Sandy Clay		14.3											
	8.0		Sandy Clay		22.7											
	1.0		Sandy Clay		23.7											
	2.0		Sandy Clay		19.0											
	3.0		Sandy Clay		23.0											
BH2	4.0		Sandy Clay		31.2											
БПZ	5.0		Sandy Clay		32.0											
	6.0		Sandy Clay				4									
	7.0		Sandy Clay													
	8.0		Sandy Clay													
	1.0		Sandy CLAY		20.0											
	2.0		Sandy CLAY		23.2											
BH3	3.0		Sandy CLAY				4									
	3.0		Sandy CLAY		26.7											
	4.0		Sandy CLAY													



	(m)	( mc			(%)	(6		nsity				(%		(%) Pa	assing	
Location	Layer Depth From (m)	Layer Depth To (mm)	Material	USC (AS1726)	Moisture Content (%)	Permeability (x10 <sup>-9</sup> )	Emerson	Maximum Dry Density	OMC	Liquid Limit	Plasticity Index	Linear Shrinkage (%)	0.075mm	0.425mm	2.36mm	19.0mm
внз	5.0		Sandy CLAY		29.5											
ытэ	6.0		Sandy CLAY		27.9											
	1.0		Sandy CLAY		18.6											
	2.0		Sandy CLAY				4									
	3.0	4.0	Sandy CLAY	CI	27.5		4			55	31	14.0	72	87	93	100
BH4	4.0		Sandy CLAY		13.4	4x10 <sup>-11</sup>										
БП4	5.0		Sandy CLAY		23.9											
	6.0		Sandy CLAY		27.4											
	7.0		Sandy CLAY		32.3											
	8.0		Sandy CLAY													
	1.0		Sandy CLAY		20.6											
	2.0		Sandy CLAY		7.0											
	3.0		Sandy CLAY				4									
	4.0		Sandy CLAY		21.6											
DUE	5.0		Sandy CLAY		29.0											
BH5	6.0		Sandy CLAY				4									
	7.0		Sandy CLAY		28.4	3x10 <sup>-10</sup>										
	6.0	7.0	Sandy CLAY	СН						52	29	12.5	75	91	98	100
	7.0		Sandy CLAY													
	8.0		Sandy CLAY		20.7											
DUC	2.5	6.0	Sandy CLAY	СН						51	32	14.0	65	88	96	100
BH6	6.6	8.0	Clayey Sand	SC		5x10 <sup>-6</sup>	4	1.904	10.7	31	19	7.0	32	77	100	100
	1.0		Sandy CLAY		15.4											
	2.0		Sandy CLAY				4									
<b>D</b> L 10	2.5	4.0	Sandy CLAY	СН						50	32	14.0	58	81	92	100
BH8	3.0		Sandy CLAY		23.3.	1x10 <sup>-10</sup>										
	4.0		Sandy CLAY		18.0											
	5.0		Sandy CLAY		26.1											
	6.0		Sandy CLAY				4									
BH8	7.0		Sandy CLAY		32.3											

Notes: DCP: Dynamic Cone Penetrometer; CBR: California Bearing Ratio; OMC: Optimum Moisture Content



# 6. Rainfall Data

The following is a summary of the rainfall data for the Torquay Golf Club. Refer to Appendix D for full details

Year	Month	Maximum Daily Rainfall
2002	2	90
2005	2	88.4
2001	4	70
1987	12	61.2
1978	11	58.6
2001	3	56
1981	5	55.4
2001	4	50
2010	3	48
1988	11	45
1988	1	42
1989	3	40.6
1981	10	40.4
1987	10	39.2
2005	8	39.2
1977	5	38.6
2004	11	38.2
1989	4	38
2000	10	38
2008	12	37.4

# 7. Geotechnical Assessment

### 7.1 Geotechnical Material Properties

The following Geotechnical material properties have been determined from the field and laboratory testing and with correlation with AS1726 and published books and journals.

Table 5.1	Geotechnical	Material	properties
10010 011	ocorconnical	material	properties

Material	Unit Weight (kN/m <sup>3</sup> )	Cohesion (kPa)	Friction Angle (°)
Sandy CLAY	20	10	25
Clayey Sand	18	2	30



#### 7.2 Slope/W Assessment

Material	Section	Dam Level	Embankment Slope	Factor of Safety	Assessment
Sandy Clay	A-A	Existing	1:3.5	2.772	Stable
Sandy Clay	A-A	Crest	1:3.5	2.772	Stable
Sandy Clay	B-B	Existing	1:3.7	2.999	Stable
Sandy Clay	B-B	Crest	1:3.7	2.977	Stable
Sandy Clay	C-C	Existing	1:3.3	2.975	Stable
Sandy Clay	C-C	Crest	1:3.3	2.923	Stable
Sandy Clay	D-D	Existing	1:2.6	3.367	Stable
Sandy Clay	D-D	Crest	1:2.6	3.367	Stable
Sandy Clay/Clayey Sand	E-E	Existing	1:1.9	1.953	Stable
Sandy Clay/Clayey Sand	E-E	Crest	1:1.9	1.963	Stable

The Slope/W Assessment were undertaken on the existing and worst case scenario with the water raising to the top of the crest level. Although this will never happen due to the design of the dam, the dam stability assessment used this as a worst case scenario trial basis. In both instances and with all sections the Slope/W assessment found the dam walls to be stable (Refer to Appendix E)

## 8. Discussion

#### 8.1 Foundations

The foundations for the dam were found to be suitable for the design type of the dam.

#### 8.2 Typical Design Slopes

The constructed design and well below the typical maximum deign limits as recommended by published documents such Farm Darms (Lewis, 2002), Design and Construction of Small Earth Dams (Nelson, 1995)

#### 8.3 Overflow

There is no risk of overflow at its current design

#### 8.4 Structural Integrity

The geotechnical investigation found that dam was stripped and keyed into the Sandy CLAY/Clayey SAND material and was compacted well.

#### 8.5 Classification of Soils

The wall was constructed of Sandy Clay that had a moderate plasticity and a very low permeability

#### 8.6 Permeability & Moisture Content of Dam

The Sandy Clay had a very low permeable material. Typically for dams the minimum requirement for the permeability is less than  $1 \times 10^{-9}$ . The four samples taken met this requirement. The moisture



content of the soils found all the samples were dry to moist. No samples or field observations found the soil to be saturated. No evidence of seepage through the dam was observed.

#### 8.7 Dispersion

This test, developed by Emerson (1967), classifies soil aggregates on the basis of their coherence in water. The interaction with water of clay-sized particles in aggregates may largely determine the structural stability of a soil. The Emerson Aggregate Test is a simple physical test for dividing aggregates into eight main classes.

The laboratory testing found that the Emerson Class was 4 and is not susceptible to tunnel erosion.

#### 8.8 Shrinkage and Cracking of Wall

For earthwork construction, linear shrinkage is used to predict instability due to crack formation through walls or potential leaking problems caused by low clay activity.

The laboratory testing found the material to have a medium shrink-swell potential and is susceptible to minor shrinkage on drying and swelling on wetting.

#### 8.9 Trees

The trees will have no significant detrimental effect on the structural integrity of the dam.

## 9. **Recommendations**

The integrity of the structure and the design of the dam at 1075 Horseshoe Bend Road is sound and meets the requirement of the intended use. It is recommended that walls and crest of the dam be topsoiled with inspections as required.

#### 9.1 Topsoil

Prior to the placement of topsoil onto the compacted embankment, the surface should be roughened to assist in combining the different soil types. Topsoil should be placed over the entire embankment to a depth of at least 200 mm and grassed with a good holding grass.

The purpose of the topsoil cover is to:

- reduce surface erosion on either side of the batter slope;
- minimise surface cracking in the embankment;
- lessen the tendency of the surface material in contact with storage water being dispersed;
- lessen wide fluctuations in embankment moisture content.

#### 9.2 Supervision

The purpose of a dam safety surveillance program is to avoid failure of the dam, by giving early warning of any kind of symptom of trouble as early as possible. At this site however, the risk of dam failure at its current design is negligible.

It is therefore recommended that a quick visual inspection be undertaken by the owner on a monthly basis looking for variations to the dam with photos taken at each inspection.



If required a comprehensive inspection by a suitably qualified engineer can be under on a yearly basis.

# Disclaimer

The findings and conclusions contained in this Report are made based on site conditions that existed at the time this work was conducted. The conclusions presented in this report are relevant to the conditions of the site and the state of legislation currently enacted as at the date of this report.

Findings and conclusions are made assuming that the soil, groundwater, geological and chemical conditions detailed within this report are accurate and remain applicable to the site at the time of writing. No other warranties are made or intended.

AGT has used a degree of skill and care ordinarily exercised by reputable members of our profession practicing in the same or similar locality.

does not make any representation or warranty that the conclusions in this report will be applicable in the future as there may be changes in the condition of the site, applicable legislation or other factors that would affect the conclusions contained in this report.

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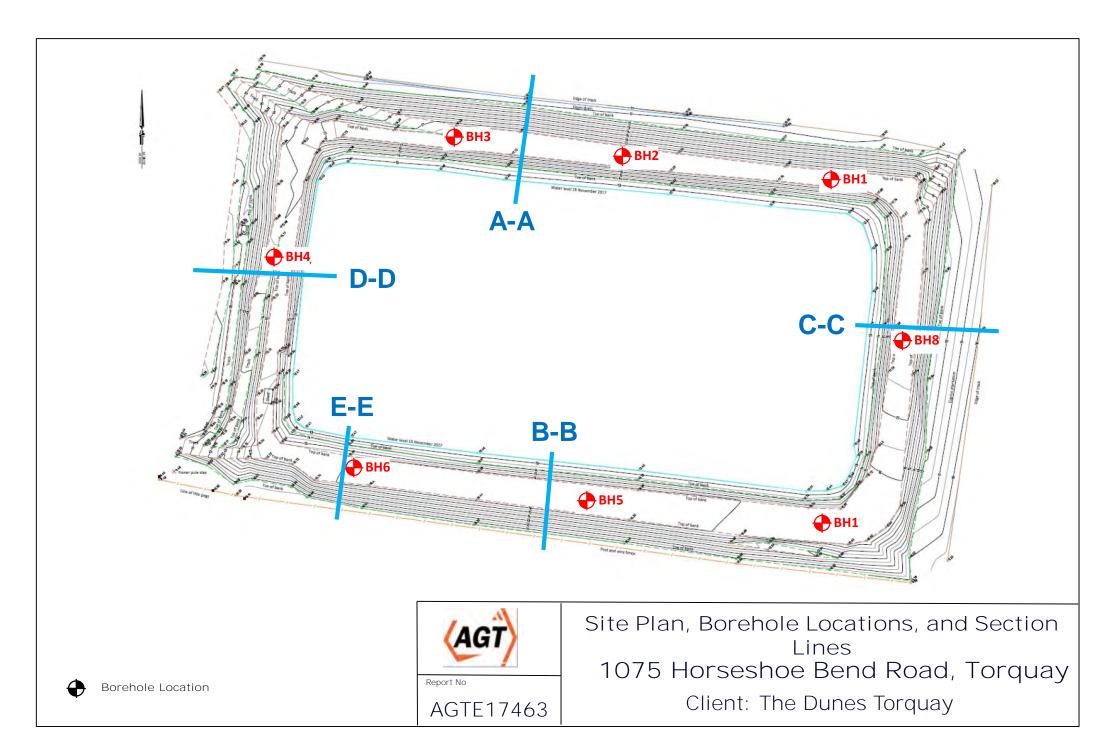
M/L

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# Appendix A – Site Plan





# **Appendix B – Engineering Logs**



BOREHOLE No



Р	RO	JE	CT:		1075 Horse Bend Road								F	PR	OJ	EC	т	NC	):					A	GTE	17	460	63		
L	ос	AT	ION:		Torquay								[	DA.	ΤE	0	FE	30	RE	HC	DLI	E:		<b>8</b> . '	11.2	201	7			
С	LIE	INT	Г:		The Dunes Torquay								l	_00	GG	E	DE	BY:						М	N					
6	Chai	nage	e:		Direction:			с	offse	et						L	.atit	ude	: -	38.3	039	19		Lo	ongiti	ude:	144	.347	087	
		it	_	ç			11		Ê				Т	ests	% p	ass	ing													
Method	Depth (m)	Depth of Unit	Graphic Log	Classification Symbol	Material Description	Moisture Condition	Consistency / Strength	Sample ID	DCP (per 100mm)	FIELD CBR	PP (kPa)	SV (kPa)	MC (%)	75µm	0.425mm	2.36mm	19mm	37.5mm			0	CBR	SWELL	OMC	MDD	Additive	ucs	OMC - Add	MDD - Add	Water
Ź	Ō	Δ	о ХХХ	ပတ်	FILL, Sandy CLAY: brown	≥ŭ M	ර ග VSt	ű	ă	Ē	Ē	Ś	Σ	75	ö	5	16	37	Η	₫	LS	Ū	ίο Ο	0	Σ	Ă	Š	0	Σ	3
											450																			
	1				- grey mottled orange			SPT			450		19.1																	
	-							2,3,3 N=6																						
	2				- orange-brown			SPT			450		18.7																	
	-							3,5,7 N=12	-																					
	3																													
	<u> </u>							SPT 3,6,7 N=13			310		25.4	57			100		58	36	12.5	5								
								N=13																						
	4																													
Solid Auger	4							SPT 2,2,3 N=5			320											-								
Solid ,								N=5																						
	5			•																										
					- brown-grey						350		31.8																	
	6																													
					- grey-brown			SPT 3,5,8 N=13	1		400		22.7 20.2	60			100		39	21	10									
								N=13																						
	-7																													
		7.05		CI	- orange-brown Sandy CLAY: orange-brown	_/ м	VSt	SPT 6,6,10 N=16	1		450		14.3									]								
			<u> </u>	+				01 = <i>n</i>	+																					
	8			+																										
								SPT 4,8,10 N=18			500		22.7																	
┝	-	8.5	<u> </u>	<b>†</b>	End of BH1 at 8.50m			N-10	╞													$\vdash$	-					-	_	╞
	9																													
L																														
					This log should be read in conju	inction v	ith the	Australian	Geot	techr	nical	Test	ing l	_og S	Sumi	mar	y Sh	eet a	and	the S	Site	Plar	۱							

BOREHOLE No



# BH2

Ы	RC	JE	CT:		1075 Horse Bend Road								Ρ	RC	DJE	С	ΓN	0:					A	GTE	17	46	63		
L	C	AT	ION:		Torquay								D	)AT	ΈC	ΟF	BC	DR	EH		<b>8</b> . '	11.2	201	7					
С	LIE	ENT	:		The Dunes Torquay								L	00	GGE	ED	ΒY	<b>'</b> :					М	N					
0	Chai	nage	e:		Direction:			o	ffse	t						La	tituo	de:	-38.	3041	05		Lo	ongitu	ıde:	144	.347	08	
		t		c			/						Те		% pa	ssin	g		Τ		1	1							
Method	Depth (m)	Depth of Unit	Graphic Log	Classification Symbol	Material Description	Moisture Condition	Consistency	Sample ID	DCP (per 100mm)	FIELD CBR	PP (kPa)	SV (kPa)	MUC (%)		0.425mm 2 36mm		19mm 37.5mm	1	H IA	LS	CBR	SWELL	OMC	MDD	Additive	UCS	OMC - Add	MDD - Add	Water
					FILL, Sandy Clay: orange-brown mottled grey	M	VSt			3	850																		
								SPT 4.3.3		ŧ	500	23	3.7																
	-							4,3,3 N=6																					
	2				- yellow-brown, white			SPT 2,2,4 N=6		4	150	1	9																
Auger	3				- yellow-orange, red			SPT 3,4,4 N=8	-	4	180	2	23																
Solid Auger								N=8																					
	_ <b>4</b> 				- orange-brown, trace gravel			SPT 2,4,5 N=9		3	350	31	1.2																
	5							SPT 2.4.6		3	850	3	82																
	6							2,4,6 N=10																					
		6.1		CI	Sandy CLAY: orange-brown	М	VSt																						
	7	6.5			End of BH2 at 6.50m																								
	_8																												
	     9																												
L																													
					This log should be read in conjun	ction w	<i>i</i> ith the	Australian	Geot	echni	cal T	Festin	g Lo	og S	umm	ary	Shee	et an	d the	Site	Plar	n							



**BOREHOLE No** 

B	Η	3

#### PROJECT: 1075 Horse Bend Road PROJECT NO: AGTE174663 LOCATION: Torquay DATE OF BOREHOLE: 8.11.2017 CLIENT: The Dunes Torquay LOGGED BY: ΜN Chainage: Direction: Offset Latitude: -38.304129 Longitude: 144.349075 Tests % passing Classification Symbol Consistency / Strength DCP (per 100mm) FIELD CBR Depth of Unit Graphic Log OMC - Add MDD - Add Sample ID Depth (m) Moisture Condition РР (кРа) SV (kPa) 0.425mm 2.36mm 37.5mm Additive Method MC (%) CBR SWELL OMC 19mm 75µm Water MDD ncs Material Description 리티 N FILL, Sandy Clay: brown-orange 600 1 SPT 4,3,3 N=6 600 20 2 500 23.2 - yellow-orange, brown, grey SPT \_ 2,3,3 N=6 3 Solid Auger - orange-brown SPT 2,4,4 N=8 450 26.7 -4 SPT 2,3,5 N=8 520 5 SPT 4,4,6 N=10 - thin sand layers 550 29.5 \_ 6 SPT 7,12,14 N=26 27.9 600 6.1 CI Sandy CLAY: orange-brown \_ 6 End of BH3 at 6.50m 7 8 9 --10

This log should be read in conjunction with the Australian Geotechnical Testing Log Summary Sheet and the Site Plan

BOREHOLE No



# BH4

Р	RO	JE	CT:		1075 Horse Bend Road								F	R	JI	EC	т	NC	):					A	GTE	17	46	63		
L	oc	AT	ION:		Torquay								C	)A <sup>-</sup>	ΤE	O	FE	30	RE	HC	DLE	Ξ:		8.1	11.2	201	7			
С	LIE	ΕNT	Г:		The Dunes Torquay								L	.00	GG	E	DE	BY:						М	N					
(	Chai	nag	e:		Direction:			o	ffset							L	.atit	ude	: -:	38.3	0359	99		Lo	ngitu	ude:	144	.349	743	
Method	Depth (m)	Depth of Unit	Graphic Log	Classification Symbol	Material Description	Moisture Condition	Consistency / Strength	Sample ID	DCP (per 100mm)	FIELD CBR	PP (kPa)	SV (kPa)	()		0.425mm %	2.36mm 88	19mm 19	37.5mm	LL	Ы	LS	CBR	SWELL	OMC	MDD	Additive	ucs	OMC - Add	MDD - Add	Water
Solid Auger N		7.6		CI	FiLL, Sandy Clay: brown, grey, white, orange         - orange-brown, mottled red, grey         - brown-orange, grey, some fine sand         - orange-brown, mottled grey, red         Sandy CLAY: orange-brown         End of BH4 at 8.50m	M	VSt	SPT 4,5,7 N=12 SPT 6,11,11 N=22 SPT 3,8,15 N=23 SPT 4,6,7 N=13 SPT 3,5,4 N=9 SPT 2,3,3 N=6 SPT 5,11,14 N=25		5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	<ul> <li>L</li> <li>L&lt;</li></ul>	18 22 11 22 21	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0		100			31			S							
	10				This log should be read in conjur	nction w	vith the	Australian	Geote	echnie	cal 1	Festin	ig L	og S	Sumr	mar	y Sh	ieet a	and	the S	Site	Plan								



**BOREHOLE No** 

B	Η	5

#### PROJECT: 1075 Horse Bend Road PROJECT NO: AGTE174663 LOCATION: Torquay DATE OF BOREHOLE: 9.11.2017 CLIENT: The Dunes Torquay LOGGED BY: ΜN Chainage: Offset Longitude: 144.348326 Direction: Latitude: -38.302764 Tests % passing Classification Symbol Consistency / Strength DCP (per 100mm) FIELD CBR Depth of Unit Graphic Log Sample ID OMC - Add MDD - Add Depth (m) Moisture Condition PP (kPa) SV (kPa) 0.425mm 2.36mm 37.5mm Additive MC (%) SWELL Method 75µm 19mm Water OMC MDD UCS CBR Material Description 리티 S VSt FILL, Sandy Clay: orange-brown Μ - orange brown mottled grey 600 1 SPT 3,5,6 N=11 450 20.6 2 - bown orange mottled, red, grey SPT 350 7 4,5,7 N=12 3 - 50mm layer of sand, light grey-brown SPT 3,6,7 N=13 600 4 Solid Auger SPT 3,4,7 N=11 420 21.6 \_ 5 SPT 2,3,6 N=9 - brown orange 420 29 6 75 100 52 29 12.5 550 SPT 2,2,4 N=6 7 600 28.4 Sandy CLAY: orange-brown mottled red, grey, trace fine gravel 7.5 VSt CI Μ 8 SPT 7,11,16 N=27 600 20.7 8.5 End of BH5 at 8.50m 9 10 This log should be read in conjunction with the Australian Geotechnical Testing Log Summary Sheet and the Site Plan

BOREHOLE No



# BH6

Р	RC	JE	CT:		1075 Horse Bend Road								F	PR	OJ	EC	TI	NC	):					A	GTE	17	46	63		
L	oc	АТ	'ION:		Torquay								[	DA	ΤE	O	= E	BOF	RE	HC	DLE	Ξ:		<b>9</b> . 1	11.2	201	7			
С	LIE	ENT	Г:		The Dunes Torquay								l	_0	GG	EC	ЭB	SY:						М	N					
'	Chai	nag	e:		Direction:			o	ffset	t						L	atit	ude	: -:	38.30	0283	37		Lo	ngitu	ıde:	144	.349	305	
Method	Depth (m)	Depth of Unit	Graphic Log	Classification Symbol		Moisture Condition	Consistency / Strength	Sample ID	DCP (per 100mm)	FIELD CBR	PP (kPa)	SV (kPa)	MC (%)	E	% p	2.36mm		37.5mm				٣	ELL	C	D	Additive	S	OMC - Add	MDD - Add	ter
Met	Dep	Dep	Gra	Syr	Material Description FILL, Silty Clay: orange-brown, grey	C Q N M	USt VSt	Sar	DCI	Ë	РР	Sν	MC	75µm	0.42	2.3(	19mm	37.5	Ξ	F	LS	CBR	SWELI	OMC	MDD	Adc	NCS	Ø	MD	Water
Solid Auger	       	6.8 - <del>7.5</del>		CI	- grey mottled orange-brown - orange-brown mottled grey Sandy CLAY: grey mottled orange End of BH6 at 7.50m	M	VSt				400 500 5550 5550 5550			65			100		51	32	14									
	10		1		This log should be read in conju	nction w	, ith the	Australian	Geote	echni	cal	Test	ing l	Log S	Sum	mary	/ Sh	eet a	and t	the S	Site I	Plan								

BOREHOLE No



# BH7

Р	RC	JE	CT:		1075 Horse Bend Road								F	PR	OJE	EC	T I	NO	):					A	GTE	17	46	63		
L	oc	АТ	ION:		Torquay								C	DA	ΤE	OF	F B	OF	RE	HC	DLE	Ξ:		9.1	11.2	201	7			
С	LIE	ENT	Г:		The Dunes Torquay								L	.00	GG	EC	ЭB	Y:						М	N					
-	Chai	inag	e:		Direction:			o	ffset							L	atit	ude	: -3	38.3	026 <sup>-</sup>	19		Lo	ngitu	ıde:	144	.347	538	
		t		-			/						Т	ests	% p	assi	ing													
Method	Depth (m)	Depth of Unit	X Graphic Log	Classification Symbol	Material Description	■ Moisture Condition		Sample ID	DCP (per 100mm)	FIELD CBR	РР (кРа)	SV (kPa)	MC (%)		_	E		37.5mm	LL	Ы	LS	CBR	SWELL	OMC	MDD	Additive	UCS	OMC - Add	MDD - Add	Water
Solid Auger		2.9 3.1 6.5 8		CI	FILL, Silty Clay: orange-brown mottled         grey         FILL, Clayey Sand: grey         FILL, Sandy Clay: brown-orange         - red-brown         - orange-brown mottled grey         FILL, Clayey Sand: grey         FILL, Clayey Sand: grey         Sandy CLAY: orange-brown mottled grey         Sandy CLAY: orange-brown mottled grey	M M M	MD VSt VSt							32			100			19					1.904					
	-   -   -   10				End of BH7 at 9.00m																									
L	<u>    10                                </u>		<u> </u>		This log should be read in conjun	ction w	vith the	Australian	Geote	echni	cal <sup>-</sup>	Testi	ng L	.og S	Sumr	mary	/ Sh	eet a	and t	the S	Site	Plan				1				



**BOREHOLE No** 

B	<b>18</b>

#### PROJECT: 1075 Horse Bend Road PROJECT NO: AGTE174663 LOCATION: Torquay DATE OF BOREHOLE: 9.11.2017 CLIENT: The Dunes Torquay LOGGED BY: ΜN Chainage: Direction: Offset Longitude: 144.346743 Latitude: -38.302918 Tests % passing Classification Symbol Consistency / Strength DCP (per 100mm) FIELD CBR Depth of Unit Graphic Log Sample ID OMC - Add MDD - Add Depth (m) Moisture Condition PP (kPa) SV (kPa) 0.425mm 2.36mm 37.5mm Additive MC (%) SWELL Method 75µm 19mm Water MDD UCS CBR Material Description 리티 N FILL, Silty Clay: brown-grey М VSt 1 SPT 4,5,7 N=12 500 15.4 - orange-brown mottled grey, red 2 600 SPT 4,6,9 N=15 58 50 32 14 100 3 - orange-brown SPT 4,6,9 N=15 550 23.3 -Solid Auger SPT 2,4,2 N=6 - orange-brown mottled red, trace gravel 600 18 5 SPT 2,4,4 N=8 300 26.1 6 400 SPT - orange brown mottled red, grey, trace 4,6,7 N=13 gravel 7 SPT 7,16,17 N=33 600 32.3 7.1 $\bigotimes$ CI Sandy CLAY: orange-brown М VSt End of BH8 at 7.50m 8 9 -10



# **Appendix C Laboratory Testing**



# Moisture Content Report

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

info@ausgeotest.com.au

Client:	The Dunes Tor	rquay			Job No:	TG51066
Project:	1075 Horsesho	oe Bend Road [	Dam		Report:	1
Location:	Torquay				Test Date:	16-Nov-17
Teet No.		F10/4 0	E10/4-2			F10/4 4
Test No:		51066-2	51066-3	51066-4	51066-5	51066-6
Location	:: BH 1	BH 1	BH 1	BH 1	BH 1	BH 1
Depth:	:: 1m	2m	3m	6m	7m	8m
Moisture Content %		18.7	25.4	22.7	14.3	22.7
Material						
				L		
				<u> </u>	<u> </u>	<u>-</u>
Test No:	51066-7	51066-8	51066-9			
Location:	:: BH 4	BH 4	BH 3			
Depth:		2m	3m			
Moisture Content %		23.2	26.7			
Material	:					
Notes:						
NOICS.						
Test Method	AS1289.2.1.1			Sampling Method	As provided	
Site Selection	N/A			1 5	,	
				Approved Signatory		1 2
~	Accreditation for compliance with ISO/IE	EC 17025 - Testing	,	Approved Signatory	y fuller	1/
NATA	The results of tests, calibrations and/or r				1-	
V	in this document, are traceable to Austra	ilian / national standards			Jon Li	llecrapp
WORLD RECOGNISED	NATA Accredited	Laboratory No. 202	245	Date	e: 29-Nov-17	1



# Moisture Content Report

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

info@ausgeotest.com.au

Client:	The Dunes Tor	rquay			Job No:	TG51066
Project:	1075 Horsesho	be Bend Road [	Dam		Report:	11
Location:	Torquay				Test Date:	03-Dec-17
Test No:	51066-25	51066-26	51066-27	51066-28	51066-29	51066-30
Location:	: BH 2	BH 8	BH 5	BH 5	BH 8	BH 4
Depth:	: 4m	4m	2m	1m	<b>1</b> m	3m
Moisture Content %		14.9	<b>19.5</b>	20.6	15.4	27.5
Material:	-	14.5	19.0	20.0	10.4	27.5
			<u> </u>		<u> </u>	
Test No:	51066-31	51066-32	51066-33	51066-34	51066-35	51066-36
Location:	: BH 3	BH 4	BH 3	BH 5	BH 2	BH 3
Dopth	1m	5m	6m	4m	5m	Em
Depth: Moisture Content %		23.9	6m 27.9	4m 21.6	32.0	5m 29.5
Material:		23.7	21.7	21.0	32.0	29.0
Notes:						
[						
Test Method	AS1289.2.1.1		5	Sampling Method	As provided	
Site Selection	N/A					
	Accreditation for compliance with ISO/IE	:C 17025 - Testing	,	Approved Signatory	J. liller	12
NATA	The results of tests, calibrations and/or n				1	1
$\mathbf{V}$	in this document, are traceable to Austral	lian / national standards			Jon Lil	llecrapp
WORLD RECOGNISED	NATA Accredited	Laboratory No. 202	245	Date:	: 05-Dec-17	



# Moisture Content Report

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

info@ausgeotest.com.au

Client:	The Dunes Tor	rquay			Job No:	TG51066
Project:	1075 Horsesho	pe Bend Road [	Dam		Report:	12
Location:	Torquay				Test Date:	03-Dec-17
Test No:	51066-37	51066-38	51066-39	51066-40	51066-41	51066-42
Location:	: BH 4	BH 5	BH 1	BH 5	BH 5	BH 3
Depth:		8m	6m	5m	7m	2m
Moisture Content %		20.7	20.2	29.0	16.9	22.8
Material:		<u> </u>				
Test No:	51066-43	51066-44	51066-45	51066-46	51066-47	
Location:		BH 2	BH 2	BH 4	BH 8	+
Depth:	: 1m	2m	3m	7m	5m	
Moisture Content %	23.7	19.0	23.0	32.3	26.1	
Material:						
r						
Notes:						
[					· · · · · ·	
Test Method	AS1289.2.1.1		5	Sampling Method	As provided	
Site Selection	N/A					
<b>^</b>	Accreditation for compliance with ISO/IE	EC 17025 - Testing	/	Approved Signatory	Intillar	1
NATA	The results of tests, calibrations and/or r	measurements included			1	
	in this document, are traceable to Austra	Ilian / national standards			Jon Li	llecrapp
	NATA Accredited	Laboratory No. 202	J∕I5	Date	e: 05-Dec-17	,

Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-1 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH1 (3.0 - 4.0m)

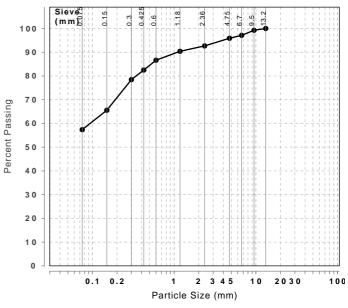
Atterberg Lim	it (AS1289 3. <sup>-</sup>	1.2 & 3.2	2.1 & 3	.3.1)	Min	Max
Preparation M	lethod			Dry Sieve		
Sample Histo	ry		C	ven Dried		_
Liquid Limit (9	%)			58		
Plastic Limit (				22		
Plasticity Inc	lex (%)			36		
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink				12.5		
Cracking Cru	mbling Curling	)		Cracking		
Particle Distri	bution (AS128	39 3.6.1)	)			
Sieve	Passed %	Passin Limits		Retained %	Retai Limits	
13.2 mm	100			0		
9.5 mm	99			1		
6.7 mm	97			2		
4.75 mm	96			1		
2.36 mm	93			3		
1.18 mm	90			2		
0.6 mm	87			4		
0.425 mm	82			4		
0.3 mm	78			4		
0.15 mm	66			13		
0.075 mm	57			8		

AGT

Australian Geotechnical Testing Warrnambool Laboratory 2/1109 Raglan Parade Warrnambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing



Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246



Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-2 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH1 (6.0 - 7.0m)

Atterberg Lim	it (AS1289 3.	2.1 & 3	.3.1)	Min	Max	
Preparation N	Preparation Method			Dry Sieve		
Sample History				Air Dried		_
Liquid Limit (9	%)			39		
Plastic Limit (	astic Limit (%)			18		
Plasticity Inc						
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink	age (%)			10.0		
Cracking Cru	mbling Curling	9		None		
Particle Distri	bution (AS128	39 3.6.1)				
Sieve	Passed %	Passing Limits			Retained Limits	
13.2 mm	100			0		
9.5 mm	100			0		
6.7 mm	98			2		
4.75 mm	96			2		
2.36 mm	94			3		
1.18 mm	92			2		
0.6 mm	89			4		
0.425 mm	83			5		
0.3 mm	78			5		
0.15 mm	65			13		
0.075 mm	60			5		

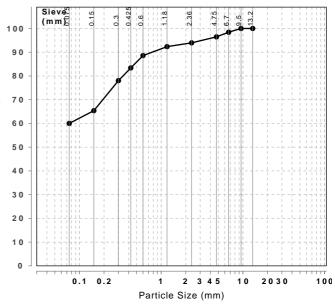


Australian Geotechnical Testing Warmambool Laboratory 2/1109 Raglan Parade Warmambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing



Percent Passing

Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246



Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-3 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH4 (3.0 - 4.0m)

Atterberg Limit (AS1289 3.1.2 & 3.2.1 & 3.3.1)					Min	Max
Preparation Method			Dry Sieve			
Sample History			C	Oven Dried		
Liquid Limit (9	%)			55		
Plastic Limit (	%)		24			
Plasticity Inc	lex (%)			31		
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink	age (%)			14.0		
Cracking Cru	mbling Curling	ļ		None		
Particle Distribution (AS1289 3.6.1)						
Sieve	Passed %	Passing Limits	g	Retained %		ned S
13.2 mm	100			0		
9.5 mm	99			1		
6.7 mm	98			1		
4.75 mm	96			2		
2.36 mm	93			3		
1.18 mm	92			2		
0.6 mm	89			2		
0.425 mm	87			3		
0.3 mm	84			3		
0.15 mm	77			7		
0.075 mm	72			5		

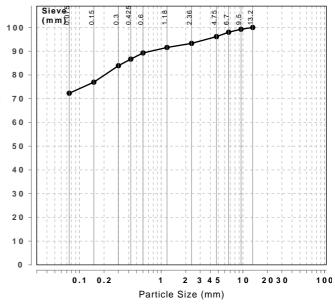


Australian Geotechnical Testing Warrnambool Laboratory 2/1109 Raglan Parade Warrnambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing



Percent Passing

Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246



Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-4 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH5 (6.0 - 7.0m)

Atterberg Limit (AS1289 3.1.2 & 3.2.1 & 3.3.1)					Min	Max
Preparation Method			Dry Sieve			
Sample History			C	ven Dried		-
Liquid Limit (9	%)			52		
Plastic Limit (	%)			23		
Plasticity Inc	lex (%)			29		
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink	age (%)			12.5		
Cracking Cru	mbling Curling	J		Cracking		
Particle Distribution (AS1289 3.6.1)						
Sieve	Passed %	Passin Limits	g	Retained %		ned S
13.2 mm	100			0		
9.5 mm	99			1		
6.7 mm	99			0		
4.75 mm	99			0		
2.36 mm	98			1		
1.18 mm	96			1		
0.6 mm	94			2		
0.425 mm	91			3		
0.3 mm	88			3		
0.15 mm	80			8		
0.075 mm	75			4		

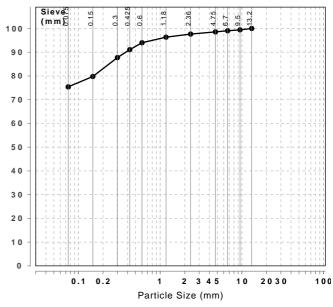


Australian Geotechnical Testing Warrnambool Laboratory 2/1109 Raglan Parade Warrnambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing



Percent Passing

Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246



Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-5 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH6 (2.5 - 6.0m)

Atterberg Limit (AS1289 3.1.2 & 3.2.1 & 3.3.1)						Max
Preparation Method			Dry Sieve			
Sample History			C	Oven Dried		_
Liquid Limit (9	%)			51		
Plastic Limit (	%)			19		
Plasticity Inc	lex (%)			32		
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink	age (%)			14.0		
Cracking Cru	mbling Curling	g		Cracking		
Particle Distribution (AS1289 3.6.1)						
Sieve	Passed %	Passin Limits	g	Retained %	Retained Limits	
13.2 mm	100			0		
9.5 mm	99			1		
6.7 mm	99			1		
4.75 mm	98			1		
2.36 mm	96			1		
1.18 mm	95			1		
0.6 mm	92			3		
0.425 mm	88			4		
0.3 mm	84			4		
0.15 mm	72			12		
0.075 mm	65			7		

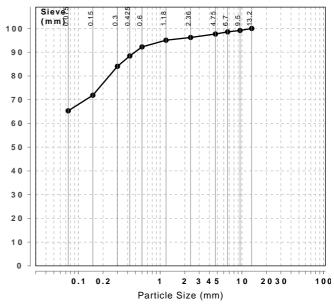
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Australian Geotechnical Testing Warrnambool Laboratory 2/1109 Raglan Parade Warrnambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing

WORLD RECOGNISED

Percent Passing

Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246



Report Number:	AGT11654-1
Issue Number:	1
Date Issued:	17/11/2017
Client:	The Dunes Torquay (AGTE)

Contact: Matt Noonan **Project Number:** AGT11654 Project Name: 1075 Horseshoes Bend Road Dam **Project Location:** The Dunes Torquay Work Request: 106 Sample Number: 11654-6 **Date Sampled:** 13/11/2017 Sampling Method: AS1289 1.2.1 6.5.4 - Machine excavated pit or trench Sample Location: BH8 (2.5 - 4.0m)

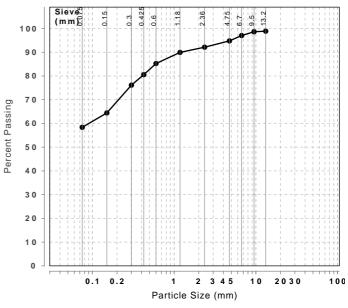
Atterberg Lim	it (AS1289 3.	2.1 & 3	.3.1)	Min	Max	
Preparation Method			Dry Sieve			
Sample History			C	ven Dried		
Liquid Limit (9	%)			50		
Plastic Limit (	%)			18		
Plasticity Inc	lex (%)			32		
Linear Shrink	age (AS1289	3.4.1)			Min	Max
Linear Shrink	age (%)			14.0		
Cracking Cru	mbling Curling	3		None		
Particle Distribution (AS1289 3.6.1)						
Sieve	Passed %	Passing Limits	g Retained %		Retained Limits	
13.2 mm	99			1		
9.5 mm	99			0		
6.7 mm	97			2		
4.75 mm	95			2		
2.36 mm	92			3		
1.18 mm	90			2		
0.6 mm	85			5		
0.425 mm	81			5		
0.3 mm	76			4		
0.15 mm	64			12		
0.075 mm	58			6		

AGT

Australian Geotechnical Testing Warrnambool Laboratory 2/1109 Raglan Parade Warrnambool Vic 3280 Phone: (03) 5023 2870 Email: danielt@ausgeotest.com.au Accredited for compliance with ISO/IEC 17025 - Testing



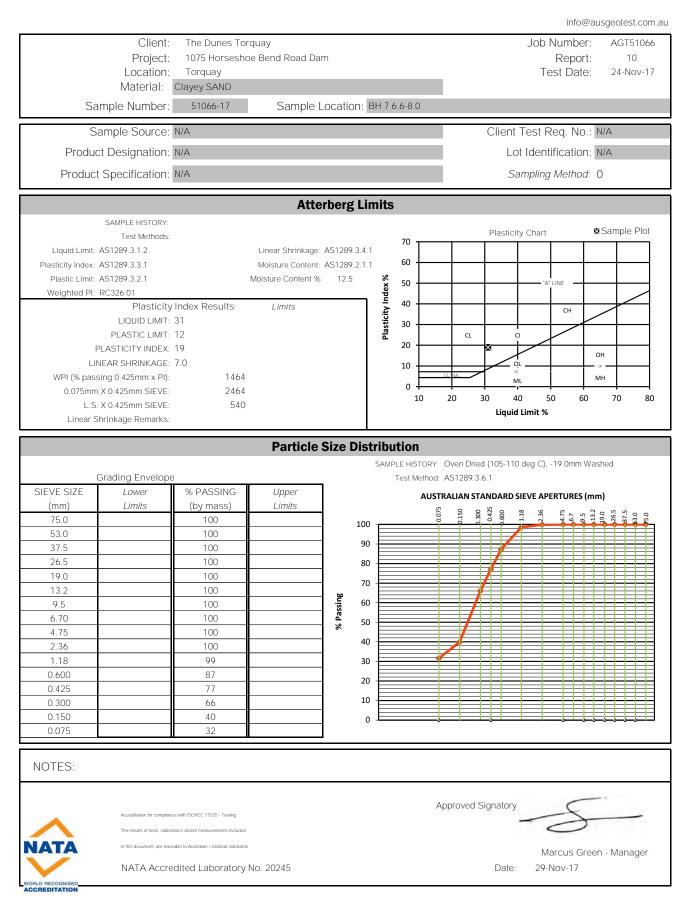
Approved Signatory: Daniel Talbot Senior Geotechnician NATA Accredited Laboratory Number: 20246





## Particle Size Distribution and Atterberg Limits Report

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583





# Permeability Report

# **Constant Head Permeability**

Australian Geotechnical Testing

21 Garden Boulevard

Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquuay		Job No: AGT51066	
Project:	1075 Horseshoe Bend Road Dam	Я	Report No: 9	
Location:	Torquay	Torquay Date of Test: 19-Nov-17		
Test Number:	51066-17			
Material Description:	Clayey SAND			
Sample Location:	BH 7 - 6.6-8.0m			
		Compaction Details	AS1289.5.1.1	
		Maximum Dry Density t/m <sup>3</sup>	1.904	
		Optimum Moisture Content %	10.7	
		Compactive Effort	Standard	
	Oversize materi	al retained on 19.0mm sieve %	0	
	Oversize materi	Dry Density Ratio Required %	98	
		Moisture Ratio Required %	100	
		Achieved Dry Density t/m3	1.904	
		Achieved Density Ratio %	100	
		Achieved Moisture Content %	10.7	
	Achieved Moisture Ratio % 100			
		Percolation Details		
		Surcharge Pressure kPa	3228.8	
		Permeant Used	Water	
Coet	fficient of Permeability	m/sec	-5E-06	
Notes:			note: 1.0E-13 = 1 x 10 <sup>-13</sup>	
Test Methods:	AS1289 1.2.1, 2.1.1, 5.1.1, AS1289.6.7.1	Sampling Method:	N/A	
		Sampling Date:	13-Nov-17	
		Approved Signatory		
	Accreditation for compliance with ISO/IEC 17025	Approved Signatory	-	
NAIA	The results of tests, calibrations and/or measurements included		-0-	
V	in this document, are traceable to Australian / national standards		Marcus Green - Manager	
WORLD RECOGNISED	NATA Accredited Laboratory No. 20245	Date:	29-Nov-17	



AS 1289.6.7.3

47 National Avenue, Pakenham VI ph 03 5943 0980 www.terrafirma			job No report No issue date	9999 9999-4 27-Nov-2017
Client:       Australian Geotechnical         Address:       21 Garden Boulevard, Di         Project:       1075 Horseshoe Bend Ro         Location:       Torquay	ngley Village, 3803		date tested tested by checked	17/11/17 - 24/11/17 PP SB
IDENTIFICATION	(AGT51066-16) BH8 - 3.0m			
SAMPLE DESCRIPTION	Silty CLAY			
PERMEANT USED	Deaired water			
CONFINING PRESSURE kPa	600			
HEAD PRESSURE kPa	590			
BOTTOM PRESSURE kPa	570			
MEAN PRESSURE kPa	20			
SPECIMEN HEIGHT	6.90	cm		
SPECIMEN DIAMETER	6.30	cm		
LENGTH TO HEIGHT RATIO	110			
DENSITY RATIO	N/A			
MOISTURE RATIO	N/A			
PERCENTAGE OVERSIZE (19.0 mm sieve)	N/A			
MOISTURE INITIAL	23.3			
MOISTURE FINAL	27.8			
PERMEABILITY M/SEC	1 x 10 <sup>-10</sup>			



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Approved Signature

S Benbow



AS 1289.6.7.3

	Avenue, Pakenham VIC : 0980 www.terrafirmala			job No report No issue date	9999 9999-3 27-Nov-2017
Client: Address: Project: Location:	Australian Geotechnical Te 21 Garden Boulevard, Ding 1075 Horseshoe Bend Rd D Torquay	ley Village, 3803		date tested tested by checked	17/11/17 - 24/11/17 PP SB
IDI	ENTIFICATION	(AGT51066-15) BH5 - 7.0m			
SAMP	PLE DESCRIPTION	Silty CLAY			
PERMEAN	NT USED	Deaired water			
CONF	INING PRESSURE kPa	600			
HE	AD PRESSURE kPa	590			
BOT	TOM PRESSURE kPa	570			
ME	AN PRESSURE kPa	20			
SPE	CIMEN HEIGHT	6.83	cm		
SPEC	IMEN DIAMETER	6.30	cm		
LEN	GTH TO HEIGHT RATIO	108			
DI	ENSITY RATIO	N/A			
MC	DISTURE RATIO	N/A			
	ENTAGE OVERSIZE 9.0 mm sieve)	N/A			
MO	ISTURE INITIAL	28.4			
MC	DISTURE FINAL	32.9			
PI	ERMEABILITY M/SEC	3 x 10 <sup>-10</sup>			



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S Benbow



AS 1289.6.7.3

	enue, Pakenham VIC 3 80 www.terrafirmala			job No report No issue date	9999 9999-2 27-Nov-2017
Address: 2 Project: 1	ustralian Geotechnical Tes 1 Garden Boulevard, Dingl 075 Horseshoe Bend Rd D orquay	ey Village, 3803		date tested tested by checked	17/11/17 - 24/11/17 PP SB
IDEN	TIFICATION	(AGT51066-14) BH4 - 4.0m			
SAMPLE	DESCRIPTION	Silty CLAY			
PERMEANT	USED	Deaired water			
CONFINI	NG PRESSURE kPa	600			
HEAD	PRESSURE	590			
BOTTO	M PRESSURE kPa	570			
MEAN	I PRESSURE kPa	20			
SPECIN	IEN HEIGHT	6.57	cm		
SPECIMI	EN DIAMETER	6.28	cm		
	H TO HEIGHT RATIO	105			
DENS	SITY RATIO	N/A			
MOIST	FURE RATIO	N/A			
	TAGE OVERSIZE mm sieve)	N/A			
MOIST	URE INITIAL	13.4			
MOIS	TURE FINAL	26.9			
	MEABILITY M/SEC	4 x 10 <sup>-11</sup>			



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LABORATORY ACCREDITATION No 15357

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Version 4 October 2016



AS 1289.6.7.3

03 5943 (	0980 www.terrafirmala	abs.com.au		report No issue date	9999-1 27-Nov-2017
Client:	Australian Geotechnical Te	-		date tested	17/11/17 - 24/11/17
Address:	21 Garden Boulevard, Ding				
Project: Location:	1075 Horseshoe Bend Rd I Torquay	Dam		tested by checked	PP SB
		(AGT51066-13) BH1 - 5.0m		checkeu	30
IDE	In the Arion				
SAMP	LE DESCRIPTION	Silty CLAY			
PERMEAN	T USED	Deaired water			
CONFI	NING PRESSURE	600			
	kPa	500			
HE	AD PRESSURE	590			
	kPa				
BOTT	OM PRESSURE	570			
	kPa				
ME	AN PRESSURE	20			
	kPa				
SPEC	CIMEN HEIGHT	6.99	cm		
SPECI	MEN DIAMETER	6.28	cm		
LENG	GTH TO HEIGHT	111			
	RATIO				
DE	NSITY RATIO	N/A			
MO	ISTURE RATIO	N/A			
	NTAGE OVERSIZE 0.0 mm sieve)				
MOI	STURE INITIAL	31.8			
МО	ISTURE FINAL	33.2			
PE	RMEABILITY				
	M/SEC	<b>2 x 10<sup>-10</sup></b>			

LABORATORY ACCREDITATION No 15357

(1

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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Report: 4
Location:	Torquay	
Sample Number: Sampling Method: Date Sampled:	: AS 1289.1.2.1.6.4(b)	Sampled By: MN Tested By: SH Date Tested: 1-Dec-17
Sample Location:	: BH 1 - 4.0m	
Material Description:	: Clayey SAND	
E	merson Class Number	4
Water Used:	Distilled Water	Water Temperature: 23 <sup>O</sup> C
Notes:	2% solution of barium chloride showed that g	jypsum is present.
Test Method:	AS1289.3.8.1	
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included in this document, are traceable to Australian / national standards	Approved Signatory
WORLD RECOGNISED		Marcus Green - Manager
ACCREDITATION	NATA Accredited Laboratory No. 20245	Date: 04-Dec-17



AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Report: 3
Location:	Torquay	
Sample Number: Sampling Method:		Sampled By: MN Tested By: SH
Date Sampled:	0.01 /17	Date Tested: 1-Dec-17
Date Sumplea.		
Sample Location:	: BH 7 - 6.5-8.0m	
Material Description:	: Clayey SAND	
	merson Class Number	4
-		4
Water Used:	Distilled Water	Water Temperature: 23 <sup>O</sup> C
Notos		
Notes:	2% solution of barium chloride showed that g	ypsum is present.
Test Method:	AS1289.3.8.1	
		Approved Signatory
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included	
V	in this document, are traceable to Australian / national standards	Marcus Green - Manager
WORLD RECOGNISED	NATA Accredited Laboratory No. 20245	Date: 04-Dec-17



AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Jok	) No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Re	port: 2
Location:	Torquay		
Sample Number Sampling Method		Sampled By: MN Tested By: SH	
Date Sampled		Date Tested: 1-Dec-17	
Sample Location	: BH 5 - 3.0m		
Material Description	Clayey SAND		
-	marcan Class Number	Λ	
-	merson Class Number	4	
Water Used:	Distilled Water	Water Temperature: 23	°C
Notes:	2% solution of barium chloride showed that	gypsum is present.	
	· · · · · · · · · · · · · · · · · · ·		
Test Method:	AS1289.3.8.1		
$\wedge$	Accreditation for compliance with ISO/IEC 17025 - Testing	Approved Signatory	
NATA	The results of tests, calibrations and/or measurements included in this document, are traceable to Australian / national standards	Ma	) Ircus Green - Manager
WORLD RECOGNISED	NATA Accredited Laboratory No. 20245	Date: 04-Dec-	



AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay		Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam		Report: 8
Location:	Torquay		
	510// 01		
Sample Number: Sampling Method:		Sampled By: MN Tested By: SH	
Date Sampled:	0/01 /47	Date Tested: 1-Dec-17	
Date Sampled.			
Sample Location:	BH 3 - 3.0m		
Material Description:	Clayey SAND		
_		4	
E	merson Class Number	4	
	-		
Water Used:	Distilled Water	Water Temperature:	23 <sup>0</sup> C
Water Useu.		water remperature.	25
Notes:			
	2% solution of barium chloride showed that	yypsum is present.	
Test Method:	AS1289.3.8.1		
			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing	Approved Signatory	5
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WORLD RECOGNISED	NATA Accredited Laboratory No. 20245	Date: 0	4-Dec-17



AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Report: 7
Location:	Torquay	
Sample Number:	: 51066-23	Sampled By: MN
Sampling Method:		Tested By: SH
Date Sampled:	0.01 /17	Date Tested: 1-Dec-17
Sample Location:	: BH 2 - 6.0m	
Material Description:	Clayey SAND	
	merson Class Number	4 Water Temperature: 23 <sup>o</sup> C
Notes:	2% solution of barium chloride showed that g	ypsum is present.
Test Method:	AS1289.3.8.1	
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included in this document, are traceable to Australian / national standards	Approved Signatory
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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay		Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam		Report: 6
Location:	Torquay		
Sample Number:		Sampled By: MN	
Sampling Method:	0.01 /17	Tested By: SH Date Tested: 1-Dec-17	
Date Sampled:	7/1007/17	Dale resieu. r-Dec-17	
Comple Legation	BH 8 - 2.0m		
Sample Location:	ВП 8 - 2.011		
Material Description:	Clayey SAND		
	ſ		
E	merson Class Number	4	
	· · · ·		
Water Llood.	Distilled Water	Water Temperature	22 00
Water Used:	Distilled Water	Water Temperature:	23 <sup>o</sup> C
Notes:			
	2% solution of barium chloride showed that g	ypsum is present.	
TechNahad	AC1000.0.0.1		
Test Method:	AS1289.3.8.1		
A		Approved Signatory	
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included		5
V	In this document, are traceable to Australian / national standards		Marcus Green - Manager
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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Report: 5
Location:	Torquay	
Sample Number		Sampled By: MN
Sampling Method	0.01 /47	Tested By: SH Date Tested: 1-Dec-17
Date Samplec	2: 9/1007/17	
Sample Location	n: BH 5 - 6.0m	
Material Description	n: Clayey SAND	
-		Λ
E	merson Class Number	4
Water Used:	Distilled Water	Water Temperature: 23 <sup>O</sup> C
Notes:	20% colution of barium oblarido abouted that	
	2% solution of barium chloride showed that g	ypsum is present.
Test Method:	AS1289.3.8.1	
		$\subset$
$\sim$	Accreditation for compliance with ISO/IEC 17025 - Testing	Approved Signatory
NATA	The results of tests, calibrations and/or measurements included in this document, are traceable to Australian / national standards	Marcus Green - Manager
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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam	Report: 13
Location:	Torquay	
Comple Number	51066-10	Sampled By: MN
Sample Number: Sampling Method:		Sampled By: MN Tested By: MG
Date Sampled:	0/01 /17	Date Tested: 5-Dec-17
Sample Location:	BH 4 - 2.0m	
Material Description:	Clayey SAND	
E	merson Class Number	4
	l	
Water Used:	Distilled Water	Water Temperature: 24 <sup>O</sup> C
Notes:		
	2% solution of barium chloride showed that g	ypsum is present.
Test Method:	AS1289.3.8.1	
$\wedge$		Approved Signatory
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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay	Job No: AGT51066	_
Project:	1075 Horseshoe Bend Road Dam	Report: 15	
Location:	Torquay		
Sample Number:	: 51066-20	Sampled By: MN	
Sampling Method:		Tested By: MG	
Date Sampled:	: 9/Nov/17	Date Tested: 5-Dec-17	
Sample Location:	: BH 4 - 3.0m		
Material Description:	: Clayey SAND		
Water Used:	merson Class Number	4 Water Temperature: 24 °C	
Notes:	2% solution of barium chloride showed that g	ypsum is present.	
Test Method:	AS1289.3.8.1		
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included in this document, are traceable to Australian / national standards	Approved Signatory	
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AS1289.3.8.1

Australian Geotechnical Testing 21 Garden Boulevard Dingley Village VIC 3172 PO Box 221 Hallam, VIC 3803 ph 1300 026 583

Client:	The Dunes Torquay		Job No: AGT51066
Project:	1075 Horseshoe Bend Road Dam		Report: 14
Location:	Torquay		
Sample Number: Sampling Method:		Sampled By: MN Tested By: MG	
Date Sampled:	0.01 /17	Date Tested: 5-Dec-17	
Date Sampled.			
Sample Location:	BH 8 - 6.0m		
Material Description:	Clayey SAND		
-		Λ	
E	merson Class Number	4	
Water Used:	Distilled Water	Water Temperature:	24 <sup>0</sup> C
		' L	
Notes:			
	2% solution of barium chloride showed that g	jypsum is present.	
Test Method:	AS1289.3.8.1		
$\wedge$		Approved Signatory	C
NATA	Accreditation for compliance with ISO/IEC 17025 - Testing The results of tests, calibrations and/or measurements included	-	3
$\mathbf{\vee}$	in this document, are traceable to Australian / national standards		Marcus Green - Manager
ACCREDITATION	NATA Accredited Laboratory No. 20245	Date: 0	5-Dec-17



# Appendix D – Rainfall Data

# Daily Rainfall (millimetres)

## TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

1974	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st												0
2nd												0
3rd												0
4th												0.8
5th												0
6th												0
7th												0
8th												0
9th												0
10th												0.1
11th												2.1
12th												3.4
13th												0
14th												0
15th												0
16th												0.6
17th												0
18th											9.0	0
19th											0	0
20th											0	3.3
21st											0	0
22nd											0	0
23rd											0	0
24th											0	0
25th											0	0
26th											0	0
27th											0.2	7.6
28th											0.6	4.6
29th											1.4	0.6
30th											1.0	0
31st												0
Highest daily											9.0	7.6
Monthly Total								1			12.2	23.1

 $\downarrow$  This day is part of an accumulated total Quality control: 12.3 Done & acceptable, 12.3 Not completed or unknown

Product code: IDCJAC0009 reference: 33779642



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## Daily Rainfall (millimetres)

## TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest daily	42.0	90.0	56.0	70.0	38.6	25.0	30.8	39.2	35.8	40.4	45.0	61.2
Date of highest daily	1st 1988	8th 2002		23rd 2001	6th 1977	9th 1998	10th 1981		22nd 1976	3rd 1981	22nd 1988	2nd 1987

## Statistics for this station calculated over all years of data

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.



Product code: IDCJAC0009 reference: 33779642 Created on Sat 09 Dec 2017 20:07:08 PM EST

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

					Key	: Units = n	nm 12.3 =	Not qualit	y controlle	ed. ↓ = Par	t of accum	ulated to
2016	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	12.0	0	7.5					
2nd	0	0	0	0	Ļ	0	0					
3rd	0	2.6	0	0	Ļ	0	0					
4th	0	0.6	0	0	2.5 3 days	6.5	2.5					
5th	0	0	0	0	0	Ļ	1.5					
6th	0	0	0	5.0	0	<b>3.0</b> 2 days	23.0					
7th	0	0	1.0	3.0	0	0	0					
8th	0	0	0	0	Ļ	Ļ	8.0					
9th	0	0	0	0	3.5 2 days	<b>4.5</b> 2 days	0					
10th	0	0	3.0	0	28.0	2.0	0					
11th	0	0	4.0	0	3.0	Ļ	4.5					
12th	1.0	0	0	Ļ	1.5	4.0 2 days	0					
13th	0	0	0	2.5 2 days	0	0	16.5					
14th	1.0	0	0	0	0	0	1.0					
15th	0	0	0	0	0	0	0					
16th	0	0	0	Ļ	0	0	0					
17th	0	0	0	1.5 2 days	6.0	3.5	0					
18th	0	1.0	26.0	0	0	5.5	0					
19th	0	0	Ļ	0	0	0	0					
20th	1.0	0	2.0 2 days	0	2.5	1.5	0					
21st	0	0	0	0	0	1.5	0					
22nd	0	0	0	5.0	0	1.0	24.0					
23rd	12.0	1.0	0	0	3.0	4.0	9.0					
24th	0	0	0	0	3.0	6.0	0					
25th	1.0	7.5	0	0.5	0	Ļ	0					
26th	0		0	0	Ļ	7.0 2 days	7.5					
27th	0		0.5	0	12.5 2 days	0						
28th	17.0		0	0	Ļ	0						<u> </u>
29th	1.0		0	1.0	2.5 2 days	0						
30th	9.0		0	6.0	0	4.0						
31st	3.0		0									1
Highest Daily	17.0	7.5	26.0	6.0	28.0	6.5	24.0					<u> </u>
Monthly Total	46.0	12.7	36.5	24.5	80.0	54.0	105.0					

Annual total for 2016 = n.a

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	: Units = n	nm 12.3 =	Not quality	controlle	d. ↓ = Par	t of accum	ulated to
2010	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	9.6	22.0	0.6	0	0	0	0	5.2				
2nd	0	0	0	0	0	0	0	11.2				
3rd	0	0	0	0	0	0	0	2.0				
4th	0	0	0	0	0	0	0	0				
5th	0	12.2	0	0.6	3.2	0	0	8.8				
6th	0	0	48.0	0	1.2	8.2	0	2.0				
7th	0	0	7.0	11.0	0	1.0	0	0				
8th	0	0	19.0	1.4	2.2	0	0	0				
9th	0	0	3.6	0	0	0	0	0				
10th	0	0	0	Ļ	0	5.2	0	0				
11th	0	0	0	Ļ	4.2	0	Ļ	Ļ				
12th	0	15.0	0	2.6 3 days	3.0	Ļ	5.0 2 days	<b>30.4</b> 2 days				
13th	Ļ	0	0	0	2.5	Ļ	0	3.2				
14th	Ļ	0	0	0	3.0	Ļ	4.4	0				
15th	Ļ	6.0	0	0	2.0	9.8 4 days	9.8	Ļ				
16th	Ļ	0	0	0	0	0	1.2	6.4 2 days				
17th	Ļ	0	0	0	0	5.2	0	0				
18th	7.8 6 days	0	0	0	0	4.0	0	0				
19th	5.8	0	1.0	0	0	0.6	0.8	10.0				
20th	0	0	0	0	0	2.2	0	2.6				
21st	0	0	0	1.2	4.6	0	1.5	Ļ				
22nd	0	0	0	0	0	0	0.6	<b>2.2</b> 2 days				
23rd	0	0	0	2.0	0	0	0	0				
24th	0	0	0	5.5	0	0	0	0				
25th	0	0	0	0	0.5	5.0	0	6.6				
26th	0	0	0	0	2.5	6.8	1.0	0.5				
27th	0	0	Ļ	0	0	3.8	0	2.8				
28th	0	0	Ļ	0	0	0	0	1.0				
29th	0		10.8 3 days	1.5	Ļ	0	7.0	0				
30th	0		0	0	6.0 2 days	15.2	1.0	0				
31st	0		0		0		9.2	0				
Highest Daily	9.6	22.0	48.0	11.0	4.6	15.2	9.8	11.2				
Monthly Total	23.2	55.2	90.0	25.8	34.9	67.0	41.5	94.9				

Annual total for 2010 = n.a

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	<b>42.0</b> 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	<b>45.0</b> 22nd 1988	61.2 2nd 1987

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					Key	: Units = n	nm 12.3 =	Not quality	controlle	d. ↓ = Par	t of accum	ulated to
2009	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0.8	0	0	0	3.4	Ļ				
2nd	1.0	0	0	0	0	Ļ	7.0	Ļ				<u> </u>
3rd	0	0	0	0	0	6.0 2 days	6.4	3.8 3 days				
4th	0	0	1.0	Ļ	0	2 days 6.0	Ļ	0 0 0				
5th	0	0	6.0	Ļ	0	0	Ļ	0				
6th	0	0	4.0	1.6 3 days	0	Ļ	3.0 3 days	0				
7th	1.2	Ļ	0	1.8	0	Ļ	5.2	3.0				
8th	0	Ļ	0	0	0	Ļ	0	Ļ				<u> </u>
9th	0	1.6 3 days	0	0	0	4.0 4 days	0	Ļ				
10th	0	0 days	0	0	0	13.4	0	1.8 3 days				
11th	0	0	0	0	0	2.2	Ļ	3.0				<u> </u>
12th	0	0	0	0	0	0	13.0 2 days	2.6				
13th	0	0	10.0	0	0	0	0	0				
14th	0	0	0	Ļ	Ļ	1.4	7.4	0				
15th	0	0	7.0	Ļ	Ļ	0	0	Ļ				<u> </u>
16th	0	0	1.0	<b>4.8</b> 3 days	8.0 3 days	0	5.0	Ļ				
17th	0	0	1.4	0.2	0	0	0	3.6 3 days				
18th	0	0	0	0	0	0	0	0				
19th	0	0	0	1.2	0	0	0	0				<u> </u>
20th	0	0	0	0	0	0	0	5.6				
21st	0	0	0	0	0	Ļ	0	8.0				
22nd	0	0	0	0	0	Ļ	0	Ļ				
23rd	0	0	0	0	0	Ļ	11.2	Ļ				
24th	0	0	0	4.2	0	2.8 4 days	0.6	3.4 3 days				
25th	0	0.4	Ļ	4.8	0	0	0	5.0				
26th	0	0	6.2 2 days	5.0	14.0	0	0	10.0				
27th	0	0	0	8.0	0	0	0	0				
28th	0	0	0	7.0	0	0	0	0				<u> </u>
29th	0		0	2.0	2.0	0	2.0	Ļ				
30th	0		0	0	0	1.0	0.4	Ļ				
31st	0		0		0		2.2	20.4 3 days				
Highest Daily	1.2	0.4	10.0	8.0	14.0	13.4	11.2	10.0				<u> </u>
Monthly Total	2.2	2.0	37.4	40.6	24.0	36.8	66.8	70.2				<u> </u>

Annual total for 2009 = n.a

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	: Units = r	nm 12.3 =	Not quality	controllec	l. ↓ = Part	of accumu	lated tot
2008	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	1.0	0	0	0	0	12.3	2.2	0	0	0	2.
2nd	0	0	0	0	2.0	0	0	Ļ	1.2	0	0	(
3rd	0	0	0	2.0	1.8	0	0	2.0 2 days	5.8	0	2.0	(
4th	0	0	0	0	0	0	0	2 days	0	Ļ	0	(
5th	0	0	0	0	0	0	0	0	0	Ļ	0	2.5
6th	0	0	0	0	0	0	0	0	0	5.6	0	(
7th	0	4.5	0	0	0	0	5.6	0	0	3 days ↓	0	(
8th	0	2.7	0	0	0	1.2	5.0	0	Ļ	2.0 2 days	Ļ	(
9th	0	1.0	0	0	0	0	0	Ļ	4.2	2 days	Ļ	(
10th	0		0	0	0	3.8	Ļ	Ļ	2 days 0	0	15.2	6.4
11th	0	0	0	0	0	1.0	8.0	20.0	0	0	3 days 0	(
12th	0	0	0	0	0	0	2 days 0	3 days 4.2	0	0	0	(
13th	0	0	0	0	0	7.0	0	2.0	0	0	0	37.4
14th	0	0	0	0	0	2.0	0	0	0	0	7.4	13.8
15th	0	0	0	0	0	0	0	0	2.4	0	0	(
16th	0	0	0	0	0	0	0	Ļ	5.0	0	0	(
17th	0	0	0	0	9.0	0	0	4.0 2 days	1.8	0	0	1.6
18th	0	0	0	0	8.4	0	2.4	3.5	0	0	0	(
19th	Ļ	0	0	0	1.2	0	0	2.4	0	0	Ļ	1.2
20th	4.6 2 days	Ļ	0	0	0	3.0	5.6	0	Ļ	0	Ļ	(
21st	1.4	7.0 2 days	0	0	0	0.4	11.4	4.2	Ļ	0	<b>4.2</b> 3 days	(
22nd	0	0	0	0	0	5.4	Ļ	6.2	Ļ	2.0	7.5	(
23rd	0	1.0	0	0	0	0	Ļ	0	10.0 4 days	0	2.5	(
24th	0	0	0	0	0	7.2	Ļ	0	1.0	0	0	(
25th	0	0	Ļ	0	0	0	Ļ	0	0	0	0	(
26th	0	0.5	17.2 2 days	0	0	5.0	Ļ	0	0	0	0	(
27th	0	0	↓	Ļ	4.2	0	Ļ	0	0	0	0	1.(
28th	0	9.0	14.0 2 days	<b>5.0</b> 2 days	0	0	<b>5.6</b> 7 days	2.0	0	0	0	(
29th	0	1.2	0	↓	0	0	0	0	2.5	0	0	(
30th	0		0	3.0 2 days	0	2.0	0	0	0.5	2.2	0	4.0
31st	2.4		0		0		1.2	5.0		0		(
Highest Daily	2.4	9.0	0.0	2.0	9.0	7.2	12.3	6.2	5.8	2.2	7.5	37.4
Monthly Total	8.4		31.2	10.0	26.6	38.0	57.1	59.3	34.4	11.8	38.8	69.

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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					12		40.0	Mat available	a a m fama IV			
2007	Inn	Fab	Man	<b>A</b>			nm 12.3 = Jul	Not quality		0ct		
1st	Jan ↓	Feb 0	Mar 0	Apr 0	May 0	Jun ↓	<b>Ju</b> 5.0	Aug 1.0	Sep 0	Uci	<b>Nov</b> 0	Dec
2nd	3.0	0	0	0	0	↓ ↓	0.0	0	0	ţ	14.0	0
	2 days											
3rd 4th	0	0	0	0	5.5 4.5	↓ 9.0	4.0	2.5	4.4 0	Ļ	0 36.0	7.0
						4 days	Ļ	Ļ		Ļ		
5th	0	0	2.0	0	0	0	Ļ	Ļ	0	4.6 5 days	20.0	0
6th	0	0	0	0	7.2	4.8	Ļ	12.0 3 days	0	2.8	0	0
7th	Ļ	0	0	0	0	0	25.0 4 days	0	0	0	0	Ļ
8th	7.0	0	0	0	0	0	25.0	0	0	0	0	Ļ
9th	2 days 0	0	0	0	0	0	3.5	0	0	0	0	ļ
10th	0	0	0	0	0	0	0	4.5	3.0	0	0	4.0
11th	0	3.4	0	0	0	8.0	0	0	3.0	3.4	0	4 days
12th	0	0	0	0	0	9.0	3.6	8.0	0	Ļ	0	0
13th	0	0	0	0	0	8.0	6.7	2.0	0	↓	0	0
14th	0	0	0	0	0	0	11.6	0	0	4.0	0	0
15th	0	0	0	0	0	0	6.0	1.5	0	3 days 0	0	Ļ
16th	0	0	1.6	0	8.6	0	0	0	0	0	0	8.0
17th	0	0	0	0	0	0	Ļ	0	5.5	0	0	2 days 0
18th	0	0	0	0	4.5	19.0	12.0	Ļ	0	0	0	0
19th	Ļ	5.8	0	0	0	6.0	2 days 6.5	Ļ	0	0	0	0
20th	↓ ↓	0	0	0	0	3.0	1.5	÷ 3.0	6.0	0	0	7.0
21st	25.0	0	0	0	0	10.5	0	3 days 0	0	0	14.0	9.4
	3 days											
22nd	3.0	0	0	7.6	2.4	0	0	0	0	0	3.6	16.0
23rd	0	0	0	0	0	0	0	0	0	7.6	0	9.6
24th	0	0	9.5	0	0	0	0	0	0	0	0	Ļ
25th	0	0	8.8	0	0	0	0	0	0	0	0	Ļ
26th	0	0	2.6	0	0	0	0	0	0	3.0	1.0	Ļ
27th	0	0	0	0	0	3.0	7.0	0	4.4	0	0	3.0 4 days
28th	0	4.2	0	11.0	0	0	Ļ	0	7.6	0	0	0
29th	0		1.2	8.0	0	0	Ļ	0	9.0	0	0	0
30th	0		1.8	0	7.0	1.6	3.0 3 days	0	3.0	0	0	0
31st	0		0		7.6		0 days	0		0		0
Highest Daily	3.0	5.8	9.5	11.0	8.6	19.0	25.0	8.0	9.0	7.6	36.0	16.0
Monthly Total	38.0	13.4	27.5	26.6	47.3	81.9	120.4	34.5	45.9	25.4	88.6	64.0

#### Annual total for 2007 = 613.5 mm

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	<b>42.0</b> 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	<b>45.0</b> 22nd 1988	61.2 2nd 1987

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					Key	r: Units = r	nm 12.3 =	Not quality	controlled	l. ↓ = Part	of accumu	lated tot
2006	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0.8	0	8.4	6.2	0	0	0	0	0	0	(
2nd	9.4	7.5	0	0	21.2	2.5	3.0	0	0	0	2.5	(
3rd	0	0	0	2.0	0	2.0	1.0	1.4	0	0	0.8	(
4th	0	0	0	1.4	4.5	0	1.2	4.6	0	0	0	(
5th	0	0	0	0	1.0	0	0	0	0	1.5	0	(
6th	0	0	0	2.0	13.6	0	0.8	0	Ļ	0	0	(
7th	0	0	0	2.5	5.0	0	0	1.0	6.6 2 days	0	0	(
8th	0	0	0	1.0	1.6	0	Ļ	0	Ļ	0	0	(
9th	0	Ļ	0	0	0	0	<b>1.2</b> 2 days	0	Ļ	0	0	(
10th	0	<b>8.2</b> 2 days	0	0	1.0	0	0	0.5	5.0 3 days	0	0	(
11th	8.2	0	0	0	0	2.8	0	0	0	0	0	(
12th	0.8	0	0	0	0	0	3.6	0	0	0	0.8	(
13th	1.0	0	8.4	0	0	0	1.8	0	0	0	0	(
14th	0	0	0	0	0	0	0	0	0	0	4.0	(
15th	0	0	0	9.5	1.6	0	3.4	1.0	0	0	3.0	(
16th	0	0	0	2.5	0	Ļ	3.6	0	0	0	4.0	(
17th	0	0	0	0	0	Ļ	1.4	2.0	0	0	0	(
18th	0	0	0	0	0.5	8.2 3 days	0	0	0	0	0	(
19th	0	0	0	0	0	0	0	0	0	0	0	(
20th	0	0	0	3.0	1.6	0	0	0	5.6	0	0	(
21st	0	0	0	6.6	0	0	0	0	0	4.0	0	(
22nd	0	0	0	0	3.5	0	0	1.4	0	0	0	(
23rd	0	0	0	0	0	4.2	Ļ	0	0	0	0	4.8
24th	0	0	0	0	Ļ	0	1.8 2 days	10.0	5.2	0	0	(
25th	0	Ļ	0	0	6.4 2 days	0	0	1.8	3.0	0	0	
26th	0	6.6 2 days	0	0	0	0	0	1.8	0	0	0	20.0 2 day
27th	0	0	0	0	0	0	0	0	0	0	0	(
28th	0	0	0	0	0	0	0	0	0	Ļ	0	(
29th	6.5		0	0	2.4	0	0	0	0	<b>7.6</b> 2 days	0	(
30th	4.8		0	0	0	0.8	0	0	0	0	0	(
31st	0.8		2.0		0		3.0	0		0		(
Highest Daily	9.4	7.5	8.4	9.5	21.2	4.2	3.6	10.0	5.6	4.0	4.0	4.
Monthly Total	31.5	23.1	10.4	38.9	70.1	20.5	25.8	25.5	25.4	13.1	15.1	24.8

Annual total for 2006 = 324.2 mm

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	r: Units = n	nm 12.3 =	Not quality	controlled	. ↓ = Part	of accumu	lated tot
2005	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	1.2	1.0	3.5	0		1.8	0	(
2nd	0	26.6	0.5	0	0	0	0	0	0	0	0	(
3rd	0	88.4	0	4.0	0	0	0	0	0	0	0	9.8
4th	5.0	5.0	0	0	0	0	0	10.8	0	0	0	(
5th	3.2	0	7.0	0	0	0	0	3.8	0	0	0	(
6th	0.8	0.8		0	0	0	0	0	0	0	0	C
7th	0.2	0	0.5	0	0	0	1.5	0.4	0	0	0	26.8
8th	0	3.4	0	3.0	0	0	0	2.7	0	19.0	8.0	C
9th	0	1.8	0	0	0	7.2	3.2	0	3.0	3.4	1.4	(
10th	0	0	0	0	0	1.5	6.4	3.0	3.0	0	0	(
11th	0	0	0	0	0	12.0	2.2	4.0	0	6.3	4.1	(
12th	0	0.2	0	0	0	0	0	2.2	22.5	0	0	(
13th	0	0	0	0	0.8	0	0	0	1.0	0	0	1.5
14th	0	0	0	6.5	0	6.2	4.2	0	0	0	0	C
15th	0	0.2	0	0	0	0	Ļ	2.0	1.0	0	18.5	(
16th	0	0	1.0	0	0	3.2	<b>4.0</b> 2 days	0	4.0	0	0	C
17th	0	0	0	0	0	0	4.8	0	Ļ	0	0	C
18th	0	0	0	0	0	0	0	0	8.0 2 days	0	0	2.6
19th	0.4	0	0	0	0	4.4	0	0	1.3	0	3.0	C
20th	0	0	0	0	0	4.6	0	5.4	0.5	8.4	0.5	(
21st	0	0	0	0	0	0.2	0	0	0	2.0	0	(
22nd	0	0	0	0	0	0.8	0	7.8	0	Ļ	0	(
23rd	0	0	0	0	0	0	3.2	1.7	1.6	Ļ	0	(
24th	0	0.2	0	0	2.0	0	1.2	0.8	0.4	<b>4.4</b> 3 days	0	3.6
25th	0	0	1.2	0	0	0	6.6	0	0	0 000	0	(
26th	0	0	0	0	0.7	0	5.5	0	0	0	2.3	1.6
27th	27.4	0	0	0	2.0	0	0	0	0	1.0	0	(
28th	0	0	0.4	0	0	0	0.2	0	0	0	0	(
29th	1.4		0	1.6	0	0	0	0	10.0	0.8	0	(
30th	2.2		0	0	1.6	0	0	4.8	0.8	0	0	(
31st	0		0		1.3		0	39.2		0		(
Highest Daily	27.4	88.4	7.0	6.5	2.0	12.0	6.6	39.2	22.5	19.0	18.5	26.8
Monthly Total	40.6	126.6		15.1	9.6	41.1	46.5	88.6		47.1	37.8	45.9

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	<b>25.0</b> 9th 1998	30.8 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	<b>45.0</b> 22nd 1988	61.2 2nd 1987

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					Key	: Units = n	nm 12.3 =	Not quality	controlled	l. ↓ = Part	of accumu	lated tot
2004	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0.5	0	0	4.2	0	7.6	0	1.4	0	0	7.0
2nd	0	2.0	0	0	0.4	0	0.2	1.0	0	0	0	(
3rd	0	0	0	0	0	0	0	6.6	0	0	10.4	(
4th	0	0	0	0	0.3	0	0.5	0	6.5	2.0	0	(
5th	10.0	0	0	0	2.0	0.6	0.2	3.0	0.1	0.4	11.6	(
6th	0	0	0	0	0	0	1.2	5.0	0	0	4.2	(
7th	0.2	0	0	0	0	0	4.0	0.8	0	0.2	8.0	(
8th	2.4	0	0	0	0.8	0	2.2	0	9.2	4.4	0.6	0.8
9th	0.4	0	7.4	0	0	7.0	0	0.8	0.8	0	0	2.8
10th	0	0	4.0	0	0	9.2	0	0.8	0	0	0	1.8
11th	0	14.6	0	0.5	0	1.2	0	0	13.2	0	0.2	3.0
12th	0	5.0	0	0	0	0	2.0	0	11.2	0	38.2	2.0
13th	0	0	0	0	0	2.2	0.8	2.8	0	0	18.0	0.6
14th	0.5	0	0	0	0	4.2	0.1	7.2	1.5	0	2.4	0.6
15th	0	0	0	0	0	1.0	0.6	8.4	3.6	0.6	0.8	C
16th	0	0	0	1.2	1.2	0	0	0.8	2.4	0	0	(
17th	0	0	0	0	0	0.2	6.8	0	0	0	0	(
18th	3.0	0	0	1.0	5.2	4.4	1.4	0	0	0	0	(
19th	0	0	0	0	3.8	1.0	0.8	0	0.2	0	1.4	0.4
20th	0	0	0	0	0	8.6	0.5	0.5	0	0	0.6	(
21st	0	0	0	0	0.4	0.4	0	0	0	0	0	(
22nd	0	0	0	0	0	0.2	0	1.3	0	0	0	(
23rd	0	0	0	23.4	0	0	0	0.8	3.6	0.4	0	C
24th	0	0	0	8.6	3.4	1.2	8.6	0	0	0	0	C
25th	0.8	0	0	0.4	0	2.0	0	0	0.4	0	0	(
26th	0	0	0	0	0.6	4.4	1.6	0	0	0	0	(
27th	0	0	0	7.4	7.8	1.0	1.6	0.8	0.6	36.0	0	2.4
28th	1.4	0	0	0	1.4	0	5.0	0	0	3.8	0	4.8
29th	1.0	0.6	10.2	0	1.0	2.0	0	0	5.2	0	0	1.4
30th	6.2		3.2	1.5	0	0	0	9.8	0	0	0.2	(
31st	0		0		1.2		0	9.6		0		(
Highest Daily	10.0	14.6	10.2	23.4	7.8	9.2	8.6	9.8	13.2	36.0	38.2	7.0
Monthly Total	25.9	22.7	24.8	44.0	33.7	50.8	45.7	60.0	59.9	47.8	96.6	27.6

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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Product Code: IDCJAC0009 reference: 33799265

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					Key	: Units = r	nm 12.3 =	Not quality	controlled		of accumu	ated tot
2003	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	10.0	0	Ļ	0	1.6	0	2.4	0	4.0	0	3.4	4.0
2nd	0	0	<b>5.8</b> 2 days	0	0	1.2	0	0	1.6	24.2	2.6	C
3rd	0	0	0	0	0	0.6	0	0	0.5	1.0	0	C
4th	0	0	0	0	0	0.3	0	0	0	0.4	0	C
5th	0	0	1.2	0	0	1.8	0	0	0	0	0	2.4
6th	0	0	0	0	0	4.2	0	1.6	3.0	0	0	C
7th	0	0	0	0	0	6.2	0	0	0	0	0	C
8th	0	0	2.4	3.4	0	0	0.3	0	0	1.4	0	C
9th	0	0	1.0	0.4	0	0.3	0	5.2	0	0.2	1.0	C
10th	0	0	0	0	0	0	0	2.0	0.2	2.6	0	C
11th	0	0	0	16.0	0	0	0	2.0	1.0	2.0	0	C
12th	0	0	0	5.0	0	0	0.3	2.4	8.6	1.2	0	C
13th	0	0	0	0.8	0	1.4	1.6	8.8	0	0	0	3.0
14th	0	0	0	18.4	0	1.3	0	2.0	5.0	0	0	C
15th	0	0	0	2.4	0.5	0	0	2.2	6.0	4.2	0	C
16th	0	0	0	4.4	0.4	0	8.2	0	1.4	0	0	C
17th	0	0	0	0	0	1.0	0.3	0	0.4	0	0	C
18th	0	0	0	0	7.0	0	0	2.2	3.2	0	0	C
19th	0	0	0	0	1.4	0.4	1.0	1.4	0.4	0	0	3.6
20th	0	0	10.2	0	1.0	0.5	0	0	0	2.0	2.6	C
21st	0	6.6	4.6	0	4.5	0	0	0	0	4.5	0	C
22nd	0	17.0	5.0	0	0.3	1.0	3.8	6.0	0	2.5	0	24.0
23rd	0	0	0	0	0	1.5	0	0	0.2	5.3	11.0	C
24th	0	0	0	0.3	0	0	12.4	18.0	3.0	4.4	0	C
25th	0	0.8	0	0	0	0	11.0	9.0	4.0	0	0	C
26th	0	0	0	0	0.6	0	9.4	2.0	4.2	3.2	0	C
27th	2.4	0	0	0	0	5.0	1.0	3.8	2.4	0	0	C
28th	0	0	0	0	0	3.0	0	0	2.0	0	0	C
29th	0		0	0	0	2.0	13.0	0	0.6	10.6	0	C
30th	0.8		0	0	0	0.6	24.0	5.6	1.6	0.4	0	C
31st	6.0		0		0		0.3	3.0		17.8		(
Highest Daily	10.0	17.0	10.2	18.4	7.0	6.2	24.0	18.0	8.6	24.2	11.0	24.0
Monthly Total	19.2	24.4	30.2	51.1	17.3	32.3	89.0	77.2	53.3	87.9	20.6	37.0

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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Station: Torquay G Lat: 38.34° S	Lon: 144.3	I°E EI	evation:	Number 15 m	. 87 100	Opened	. 1974	Now: C	iheu			
					Key	/: Units = r	nm 12.3 =	Not quality	/ controlled	l. ↓ = Part	of accumu	lated tota
2002	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Νον	Dec
1st	5.0	0	0	0	0	3.0	0	0	0	0	0	C
2nd	2.0	0	0	0	0	0	0	5.0	0	0	0	C
3rd	2.0	0	2.0	0	0	0	8.0	7.0	3.0	0	2.0	C
4th	0	0	0	3.0	0	0	3.0	6.0	1.0	Ļ	2.0	C
5th	0	0	0	0	0	0	0	0	0	1.0 2 days	1.0	4.0
6th	0	0	0	0	0	0	0	0	1.0	0	0	8.0
7th	0	0	0	0	0	0	0	3.0	1.0	0	0	1.0
8th	2.0	90.0	0	0	0	1.0	3.0	2.0	0	1.0	0	0
9th	0	0	0	0	0	3.0	1.4	0	6.0	2.0	0	0
10th	0	4.0	0	0	1.0	0	0	0	3.0	0	0	0
11th	0	0	0	0	0	2.0	0	0	3.0	0	0	0
12th	0	0	0	0	0	0	0	6.0	0	0	0	0
13th	0	0	0	24.0	2.0	7.0	0	13.0	0	11.0	2.0	0
14th	0	0	0	1.0	0	3.0	0	8.0	0	5.0	0	0
15th	0	0	0	0	0	3.0	0	1.0	0	0	0	0
16th	0	2.0	0	0	7.0	1.0	0	0	5.0	0	0	0
17th	0	0	0	0	5.0	8.0	0	0	3.0	0	0	0
18th	0	0	0	0	0	5.0	0	0	1.0	0	0	0
19th	0	0	0	0	10.0	0	0	0	3.0	0	0	0
20th	0	0	0	0	10.0	0	0	0	0	0	0	0
21st	0	0	10.0	0	17.0	0	9.0	0	0	0	0	0
22nd	6.0	0	0	0	5.0	0	2.0	0	0	0	0	0
23rd	4.0	0	0	0	0	0	0	2.0	0	6.0	0	0
24th	0	0	0	0	0	0	4.0	0	0	4.0	0	0
25th	0	0	0	6.0	0	1.0	0	0	0	9.0	0	0
26th	0	0	4.0	0	0	1.0	0	0	0	0	24.0	0
27th	0	0	0	0	3.0	0	0	0	0	Ļ	0	0
28th	2.0	0	0	0	9.0	16.0	0	0	4.0	2.0 2 days	0	0
29th	0		0	0	3.0	4.0	3.3	9.0	7.0	0	0	0
30th	0		0	0	0	0	0	0	0	0	0	2.0
31st	0		0		0		0	2.0		0		10.0
Highest Daily	6.0	90.0	10.0	24.0	17.0	16.0	9.0	13.0	7.0	11.0	24.0	10.0
Monthly Total	23.0	96.0	16.0	34.0	72.0	58.0	33.7	64.0	41.0	41.0	31.0	25.0

Annual total for 2002 = 534.7 mm

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	<b>42.0</b> 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	<b>30.8</b> 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	<b>45.0</b> 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

Gaps occur in the table where a valid observation is not available. This is frequently associated with the observer being unavailable (where observations are undertaken manually), a failure in the observing equipment, or when an event has produced suspect data.
Product Code: IDCJAC0009 reference: 33799302

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

Station: Torquay Go Lat: 38.34° S	Lon: 144.3	1°E E	levation:	Number 15 m		Opened		Now: C	•			
					Key	/: Units = r	mm 12.3 =	Not quality	/ controlled	d. ↓ = Part	of accumu	lated tota
2001	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	0	0	0	7.0	0	10.0	0	C
2nd	0	0	0	0	0	0	8.0	2.0	4.0	0	0	1
3rd	0	0	0	0	0	0	0	0	0	25.0	0	16.0 2 days
4th	0	Ļ	0	0	0	0	0	0	Ļ	4.0	0	4.0
5th	2.0	25.0 2 days	0	0	0	0	0	8.0	6.0 2 days	0	0	C
6th	0	0	0	0	0	6.0	2.0	0	0	5.0	10.0	(
7th	0	0	0	0	0	6.0	14.0	0	0	3.0	0	12.0
8th	0	0	0	0	0	0	Ļ	Ļ	4.0	Ļ	3.0	C
9th	0	8.0	0	5.0	0	3.0	5.0 2 days	6.0 2 days	Ļ	Ļ	0	C
10th	0	0	0	0	0	5.0	2.0	0	6.0 2 days	Ļ	0	C
11th	0	0	0	0	0	0	0	0	0	Ļ	16.0	ļ
12th	0	0	0	0	0	4.0	2.0	0	3.0	<b>8.0</b> 5 days	10.0	2.0 2 days
13th	0	10.0	0	0	0	0	3.0	0	0	Ļ	8.0	C
14th	0	0	0	0	0	5.0	0	0	0	5.0 2 days	0	C
15th	0	0	0	0	0	7.0	0	0	0	0	0	C
16th	0	0	0	0	0	Ļ	Ļ	0	0	6.0	0	C
17th	0	0	Ļ	0	0	5.0 2 days	3.0 2 days	14.0	0	0	0	C
18th	0	0	16.0 2 days	0	10.0	0	0	10.0	0	Ļ	19.0	C
19th	0	0	0	0	0	0	4.0	Ļ	0	8.0 2 days	0	C
20th	0	0	0	0	0	0	Ļ	10.0 2 days	0	0	0	(
21st	0	0	10.0	4.0	2.0	Ļ	4.0 2 days	4.0	0	0	0	(
22nd	0	0	56.0	50.0	0	6.0 2 days	0	12.0	0	0	0	(
23rd	0	0	6.0	70.0	0	0	0	6.0	Ļ	0	0	C
24th	0	0	0	28.0	0	0	0	0	Ļ	18.0	12.0	C
25th	4.0	0	6.0	0	0	0	0	0	12.0 3 days	2.0	0	C
26th	0	0	0	0	0	0	0	0	4.0	Ļ	4.0	2.0
27th	12.0	0	0	0	3.0	0	0	0	0	<b>7.0</b> 2 days	0	6.0
28th	0	0	0	9.0	4.0	0	7.0	0	0	↓ Lags	0	6.0
29th	0		0	0	Ļ	0	0	0	0	Ļ	0	C
30th	0		0	0	5.0 2 days	0	0	0	0	<b>4.0</b> 3 days	0	C
31st	0		0		4.0		0	0		0		C
Highest Daily	12.0	10.0	56.0	70.0	10.0	7.0	14.0	14.0	4.0	25.0	19.0	12.0
Monthly Total	18.0	43.0	94.0	166.0	28.0	47.0	54.0	79.0	39.0	105.0	82.0	48.0

Annual total for 2001 = 803.0 mm

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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					Key	r: Units = n	nm 12.3 =	Not quality	controlled	l. ↓ = Part	of accumu	lated tot
2000	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	4.0	0	0	12.5	0	2.2	Ļ	0	0	9.0	0	(
2nd	0	0	0	0	0	0	Ļ	0	0	0	24.0	(
3rd	0	0	0	0	0	0	Ļ	0	0	0	0	(
4th	1.5	0	2.0	0	3.0	0	Ļ	0	0	0	0	(
5th	0	0	0		15.0	10.0	Ļ	0	11.2	0	0	(
6th	0	0	1.0	0	22.0	2.0	15.0 6 days	0	0	0	0	C
7th	0	0	2.0	0	0	18.0	0 dayo	0	0	0	0	C
8th	0	0	0	0	0	3.0	0	0	19.0	2.0	0	(
9th	0	0	0	0	0	0	0	0	0	0	0	(
10th	0	0	0	0	0	0	0	0	0	3.0	0	C
11th	0	5.5	0	0	0	0	2.6	0	8.8	0	0	C
12th	0	0	0	0	0	0	0	0	0	0	0	C
13th	0	0	0	0	0	0	0	7.0	0	0	0	C
14th	0	0	3.0	0	0	0	0	0	0	0	0	C
15th	0	0	0	0	2.0	0	0	5.8	0	Ļ	0	C
16th	3.0	0	0	4.0	0	0	0	0	0	11.4 2 days	0	0
17th	0	0	0	0	0	4.0	0	0	0	0	0	0
18th	0	0	0	0	0	0	0	0	0	Ļ	0	C
19th	0	0	0	0	0	0	16.0	0	0	Ļ	0	C
20th	0	0	0	0	0	0	Ļ	0	0	11.6 3 days	0	C
21st	0	0		0	0	4.2	5.0 2 days	0	0	0	0	C
22nd	Ļ	0	0	0	0	0	0	0	0	0	0	5.0
23rd	5.0 2 days	0	0	0	0	0	0	9.4	0	0	0	17.0
24th	0	0	0	0	0	0	2.6	3.0	0	Ļ	0	C
25th	Ļ	0	0	0	0	0	3.8	0	8.5	38.0 2 days	0	C
26th	Ļ	0	0	0	0	0	14.8	0	6.5	0	0	C
27th	15.0 3 days	0	0	0	Ļ	Ļ	6.0	0	4.0	0	0	5.0
28th	0	0	0	0	Ļ	Ļ	6.2	4.0	0	0	0	(
29th	0	0	0	0	24.0 3 days	Ļ	0	0	Ļ	0	0	C
30th	0		0	6.0	11.0	12.5 4 days	0	0	1.6 2 days	0	0	C
31st	0		0		5.8		0	7.0	2 00,0	0		C
Highest Daily	4.0	5.5	3.0	12.5	22.0	18.0	16.0	9.4	19.0	9.0	24.0	17.0
Monthly Total	28.5	5.5			82.8	55.9	72.0	36.2	59.6	75.0	24.0	27.0

Annual total for 2000 = n.a

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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					Kev	/: Units = i	mm 12.3 =	Not quality	/ controlled	d. ⊥ = Part	of accumu	lated to
1999	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	. 0	0	0		0	. 0	0	0	
2nd	0	0	0		0	0	0	0	0	0	0	
3rd	0	0	17.0		0	0	0	0	0	0	0	
4th	0	0	0		0	0	0	0	0	0	0	
5th	4.2	0	0		0	0	0	0	5.0	0	Ļ	
6th	0	Ļ	0		0		0	0	2.4	0	19.0 2 days	
7th	9.8	Ļ	0	0	0		0	Ļ	5.0	0	↓	
8th	11.0	3.0 3 days	0	0	1.5		0	Ļ	0	0	5.4 2 days	
9th	0	0	0	0	0		0	Ļ	0	0	0	
10th	0	0	0	0	0		0	10.4 4 days	3.0	Ļ	0	
11th	0	2.6	0	0	0		Ļ	0	0	15.5 2 days	0	
12th	0	5.0	0	0	0	0	Ļ	0	0	Ļ	0	
13th	0	0	0	0	0	Ļ	6.0 3 days	0	0	Ļ	0	
14th	0	0	0	0	Ļ	11.0 2 days	0	Ļ	0	Ļ	0	
15th	0	0	0	0	Ļ	0	0	20.0 2 days	0	Ļ	0	
16th	0	0	0	Ļ	Ļ	0	0	0	2.0	Ļ	0	
17th	0	4.0	0	<b>3.0</b> 2 days	<b>21.0</b> 4 days	0	0	0	0	Ļ	0	
18th	0	0	0	0	0	0	4.6	0	3.0	Ļ	0	
19th	4.5	0	0	0	0		Ļ	0	0	Ļ	0	
20th	0	0	Ļ	0	0	0	Ļ	0	0	Ļ	0	
21st	0	0	Ļ	2.0	Ļ	0	2.4 3 days	0	0	Ļ	0	
22nd	0	0	32.0 3 days	0	Ļ			0	0	Ļ	8.0	
23rd	0	0	0	0	Ļ	0	0	0	0	22.0 12 days	0	
24th	0	0	Ļ	0	11.4 4 days	0	0	0	0	0	0	
25th	0	0	Ļ	0	9.2	0	0	0	0	0	0	
26th	0	0	2.0 3 days	0	4.5	0	0	7.0	0	0	0	
27th	1.0	0	↓	Ļ	2.0	0	0	23.0	0	0	0	
28th	0	0	Ļ	Ļ	0	0	0	0	0		0	
29th	3.0		9.0 3 days	6.0 3 days	Ļ	0	0	0	0	0	0	
30th	0		1.6	0	15.5 2 days	13.0	0	0	12.4	0	0	
31st	0				1.4			0		0		
Highest Daily	11.0	5.0	17.0	2.0	9.2	13.0	4.6	23.0	12.4	0.0	8.0	
Monthly Total	33.5	14.6			66.5			60.4	32.8		32.4	

Annual total for 1999 = n.a

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	r: Units = r	nm 12.3 =	Not quality	y controlled	d. ↓ = Part	of accumu	lated tot
1998	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	0	0	0	0	0	0	0	(
2nd	0	0	0	0	1.0	0	0	0	0	Ļ	0	(
3rd	0	0	0	0	0	0	Ļ	0	0	Ļ	0	(
4th	0	0	0	0	0	0	Ļ	0	4.6	10.0 3 days	0	(
5th	0	0	0	0	0	0	7.0 3 days		0	0 days	0	(
6th	0	0	0	0	0	0	0 days		0	10.0	0	(
7th	0	0	0	0	0	0	0		0	8.0	0	(
8th	0	18.4	0	0	0	0	0		0	1.6		(
9th	0	0	0	0	0	25.0	7.8		0	0	0	(
10th	0	0	0	0	0	0	8.0		0	0	0	(
11th	0	0	0	0	0	0	0		0	0	0	(
12th	0	0	0	Ļ	0	1.8	0		Ļ	0	Ļ	(
13th	18.0	0	0	Ļ	0	0	0	6.0	11.2 2 days	Ļ	25.0 2 days	
14th	35.0	0	0	17.0 3 days	0	0	0	0	Ļ	Ļ	25.0	7.6 2 days
15th	7.4	0	5.0	0	0	0	0	0	Ļ	17.0 3 days	4.8	(
16th	0	Ļ	0	0	0	7.0	0	0	16.8 3 days	0 000	0	(
17th	0	26.0 2 days	0	0	0	0	0	0	0 000	0	0	(
18th	0	0	0	0	0	0	0	0	0	2.0	0	(
19th	0	0	0	0	0	0	0	0	0	Ļ	0	(
20th	0	0	0	22.0	9.2	0	0	0	1.0	Ļ	0	
21st	0	0	0	0	0	Ļ	3.2	3.5	0	8.0 3 days	0	
22nd	0	0	0	0	0	<b>15.8</b> 2 days	0	Ļ	Ļ	0	0	
23rd	0	0	0	0	Ļ	0	0	<b>2.2</b> 2 days	5.0 2 days	2.0	0	
24th	0	0	0	0	Ļ	4.8	0	0	↓ L dujo	6.0	0	
25th	Ļ	0	0	5.0	<b>4.2</b> 3 days	0	Ļ	0	<b>2.0</b> 2 days	0	0	
26th	24.2 2 days	0	0	Ļ	0 0	0	7.0 2 days	0	2 days 0	0	0	
27th	0	0	0	3.0 2 days	0	0	2 days 4.2	0	0		2.6	
28th	0	0	0	2 days	0	0	0	0	0		12.8	(
29th	0		0	0	0	18.0	0	0	0	0	0	(
30th	0		0	0	0	5.0	10.0	0	0	0	0	(
31st	0		3.0		0		1.6	0		0		(
Highest Daily	35.0	18.4	5.0	22.0	9.2	25.0	10.0	6.0	4.6	10.0	25.0	0.0
Monthly Total	84.6	44.4	8.0	47.0	14.4	77.4	48.8		40.6			

## Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	: Units = I	mm 12.3 =	Not quality	controlled	l. ↓ = Part	of accumu	lated tot
1997	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	6.4	0	Ļ		0	0	12.0	0	22.0	C
2nd	0	0	0	0	Ļ		0	1.0	3.0	2.0	0	C
3rd	0	0	0	0	30.0		4.0	0	8.0	0	0	C
4th	0	0	0	0	3 days 17.0		1.8	0	5.2	0	0	C
5th	↓	0	0	Ļ	0		0	0	0	0	0	4.5
6th	5.2	0	0	Ļ	0		0	0	Ļ	0	0	C
7th	2 days 0	0	0	2.0	13.8		0	0	Ļ	0	0	C
8th	0	0	0	3 days 0	3.8		0	8.8	15.0	2.0	0	C
9th	0	Ļ	0	0	0		9.8	Ļ	3 days 0	0	0	C
10th	0	÷	0	0	0		0	* ↓	0	0	0	C
11th	0	2 days 0	0	0	0		0	7.0	0	- ↓	11.6	C
								3 days				
12th	0	0	0	0	0		0	3.8	0	Ļ	0	C
13th	0	0	0	0	0		0	0	Ļ	2.2 3 days	0	C
14th	1.2	0	0	0	0		0	0	Ļ	0	18.0	C
15th	0	0	0	0	0		0	0	14.2 3 days	0	9.0	C
16th	0	0	0	0	0		5.0	Ļ	0	0	0	0
17th	0	0	0	0	Ļ		2.6	Ļ	0	0	1.4	C
18th	0	0	0	0	Ļ		0	10.4 3 days	0	Ļ	0	C
19th	0	0	0	0	11.2 3 days		0	1.4	0	Ļ	0	C
20th	0	0	0	0	0		0	0	0	7.0 3 days	0	C
21st	0	0	0	0	0		0	0	0	0	0	C
22nd	18.0	4.8	Ļ	4.0	0		0	0	0	0	0	C
23rd	14.0	0.2	Ļ	0	0		0	Ļ	0	0	0	C
24th	0	0	2.0 3 days	0	Ļ		0	Ļ	0	0	0	C
25th	1.4	0	0	0	Ļ		0	18.8 3 days	0	0	0	C
26th	6.0	0	0	0	11.8 3 days		0	0 00,0	0	0	0	C
27th	0	0.6	0	0	1.2		0	1.0	Ļ	0	0	C
28th	0	0	0	0	0		0.8	0	Ļ	0	0	C
29th	0		3.0	0	3.2		0	0	6.0 3 days	2.5	0	(
30th	0		2.8	0	2.8		0	0	0 o uays	0	3.6	C
31st	0		0		0.4		4.0	15.2		25.0		C
Highest Daily	18.0	4.8	6.4	4.0	17.0		9.8	15.2	12.0	25.0	22.0	4.5
Monthly Total	45.8	11.0	14.2	6.0	95.2	20.8	28.0	67.4	63.4	40.7	65.6	4.5

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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					Key	: Units = n	nm 12.3 =	Not qualit	y controlle	d. ↓ = Par	t of accum	ulated to
1989	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	5.0	0	0	0					
2nd	0	0	0	3.6	0	0	10.8					
3rd	0	0	0	5.4	0	0	0					
4th	30.2	0	0	0	0	0	3.4					
5th	10.6	0	0	38.0	0	0	0.6					
6th	0	0	0	0	0	0	0					
7th	0	0	0	0	0	Ļ	0					
Bth	0	5.0	4.6	0	0	Ļ	0					
9th	0	0	0	0	26.2	16.6	0					
10th	0.4	0	40.6	0	0	3 days 3.8	0					
11th	2.6	0	0	0	1.2	3.4	18.2					
12th	0	0	2.8	12.8	0	0.6	0					
13th	0	0	0	0	0	0	0					
14th	0	0	0	0	0	Ļ	0					
15th	0	15.0	0	0	0	7.6	0					
16th	0	0	0	0	0	2 days 0	0					
17th	3.6	0	0	0	0	8.2	0					
18th	0	0	0	0	0	5.2	8.0					
19th	0	0	0	0.6	0	1.2	1.6					
20th	0	0	0	0.0	0	0	2.2					
2001 21st	0	0	16.0	0	0	0	3.0					
21st 22nd	0	0	0	0		0	0					
2211u 23rd	0	0	0	0	↓ 12.6	0	0					
					2 days							
24th	0	0	0	0	0	13.2	0					
25th	0	0	0	0	0	1.8	0					
26th	0	0	0	0	0	0	0					
27th	0	0	0	0	0	0	0					
28th	0	0	8.6	15.4	0	0	0					
29th	0		0	4.4	0	0	0					
30th	0		0	4.2	Ļ	0	Ļ					
31st	0	T	0		14.0 2 days	T	15.0 2 days					
Highest Daily	30.2	15.0	40.6	38.0	26.2	13.2	18.2					<u> </u>
Monthly Total	47.4	20.0	72.6	89.4	54.0	61.6	62.8					1

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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Product Code: IDCJAC0009 reference: 33799334

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					Key	: Units = n	nm $12.3 =$	Not quality	controlled	d. ↓ = Part	of accumu	lated tot
1988	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	42.0	0	0	0	0	0	0	0	0	0	0	(
2nd	0	0	0	0	0	0	0	0	2.8	Ļ	0	3.4
3rd	0	0	0	0	0	0	0	0	0	Ļ	0	(
4th	0	0	0	0	0	0	0	0	4.6	Ļ	0	(
5th	0	0	0	0	8.6	8.2	0	0	0	Ļ	6.8	4.0
6th	0	6.4	0	0	28.4	0	0	0	0	Ļ	0	(
7th	0	0	0	0	0.6	16.6	2.2	0	0	Ļ	0	(
8th	0	0	0	0	2.0	6.6	0	6.6	0	Ļ	0	(
9th	0	0.8	0	0	0	0	0	0.2	0	Ļ	0	(
10th	11.2	0	0	0	0	0	0	0	0	Ļ	0	16.4
11th	0	0	0	0	0	3.6	0	0	14.4	<b>17.2</b> 10 days	0	(
12th	0	0	0	0	0	1.8	0	0	0	0	0	(
13th	0	1.2	0	0	0	0	0	0	0	0	0	(
14th	0.8	0	0	0	0	6.6	0	0	0	0	Ļ	(
15th	0	0	0	0	2.2	0	16.0	0	8.0	2.8	14.8 2 days	(
16th	0	0	0	0	0.8	0	0	17.8	0	0	0	(
17th	0	0	0	0	Ļ	0	0	0	0	8.0	0	(
18th	0	0	0	0	Ļ	8.4	0	0	6.4	0	0	(
19th	0	0	0	0	26.4 3 days	0	0	Ļ	0	0	0	(
20th	0	0	0	0	1.8	0	5.8	Ļ	0	0	0	(
21st	0	0	0	0	0.6	7.4	0.4	Ļ	0	0	8.2	(
22nd	0	0	0	0	0	1.4	0	Ļ	0	0	45.0	(
23rd	0	0	0	0	6.4	0	0	Ļ	0	0	20.6	(
24th	19.2	0	0	4.6	0	0	0	12.6 6 days	0	0	0.6	(
25th	1.2	0	0	0	2.0	0	8.8	0	0	0	0	(
26th	0	0	0	0	0	0	4.0	0	0	0	0	9.8
27th	0	0	0	0	0	0	2.0	0	0	0	0	8.9
28th	0	0	0	0	0	Ļ	0	4.4	19.2	0	3.2	(
29th	0	0	0	0	0	2.8 2 days	0	0	0	0	0	(
30th	0		0	0	0	3.4	0	0	0	0	0	(
31st	0		5.8		0		0	0		0		(
Highest Daily	42.0	6.4	5.8	4.6	28.4	16.6	16.0	17.8	19.2	8.0	45.0	16.4
Monthly Total	74.4	8.4	5.8	4.6	79.8	66.8	39.2	41.6	55.4	28.0	99.2	42.5

Annual total for 1988 = 545.7 mm

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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Product Code: IDCJAC0009 reference: 33799337

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					Key	/: Units = r	nm 12.3 =	Not quality	controlled	. ↓ = Part	of accumu	lated tot
1987	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	4.0	0	0	0	0	0	6.6	0	0	(
2nd	0	0	0	0	0	0	0	0	0	0	0	61.2
3rd	29.0	0	0	0	8.8	0	0	0	0	0	0	3.2
4th	24.0	0	0	0	0	0	0	0	0	0	0	(
5th	4.6	0	0	0	0	0	0	2.0	0	6.4	0	(
6th	0	0	0	Ļ	0	0	0	0	0	0	0	(
7th	0	0	0	2.6 2 days	0	0	0	0	0	0	0	(
8th	0	0	0	0	0	0	0	0	2.1	0	0	(
9th	0	0	0	2.2	0	0	0	0	0	0	19.0	(
10th	0	0	0	0	0	0	0	0	2.3	0	0	(
11th	0	0	0	0	0	0	3.0	0	0	0	0	C
12th	0	0	0	0	0	0	0	0	0	0	0	(
13th	0	0	4.8	0	20.0	5.0	0	0	0	0	0	(
14th	0	0	0	0	5.8	0	0	0	0	0	0	(
15th	0	0	0	0	7.8	3.6	8.6	0	0	0	0	(
16th	0	0	0	0	21.0	0	1.8	0	0	6.4	0	(
17th	0	0	0	0	2.6	0	2.8	2.0	0	2.0	0	(
18th	0	0	0	0	0	0	0	0	0	0	0	(
19th	0	0	2.2	0	0	1.8	5.8	0	0	39.2	0	(
20th	0	0	0	0	0	4.2	5.6	1.6	14.6	0	6.0	(
21st	0	30.4	0	0	0	0	4.0	0	0	0	0	(
22nd	0	0	0	0	0	12.6	0.6	0	0	0	0	(
23rd	0	0	0	0	0	1.2	0	0	0	0	0	(
24th	0	0	0	0	0	1.8	0	17.4	0	0	0	(
25th	4.6	0	0	0	8.6	0	0	0	0	0	Ļ	(
26th	0	0	0	0	6.0	0.8	0	0	0	0	3.2 2 days	(
27th	0	0	0	0	4.2	0	0	0	0	0	0	(
28th	0	24.0	0	0	7.2	0.8	0	0	0	0	0	11.(
29th	0		0	10.0	0.6	0	0	0	9.0	0	0	(
30th	0		0	0	0	0	16.0	0	6.2	0	0	(
31st	0		17.6		0		1.0	0		0		(
Highest Daily	29.0	30.4	17.6	10.0	21.0	12.6	16.0	17.4	14.6	39.2	19.0	61.2
Monthly Total	62.2	54.4	28.6	14.8	92.6	31.8	49.2	23.0	40.8	54.0	28.2	75.4

Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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Product Code: IDCJAC0009 reference: 33799379

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					Key	: Units = n	nm 12.3 =	Not quality	controlled	. ↓ = Part	of accumu	lated tot
1986	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	5.2	0	0	3.2	0	8.2	0	(
2nd	0	0	0	0	0	0	11.2	0	1.8	8.6	0	(
3rd	0	0	0	0	0	1.4	5.0	0	0	14.8	0	(
4th	0	0	0	0	0	0	2.6	0	0	0	0	(
5th	0	0	0	0	0	0	0	0	0	5.2	0	(
6th	0	0	0	0	0	0	0	0	0	5.2	0	(
7th	0	0	0	0	14.8	0	0	0	0	2.4	0	20.0
8th	0	0	Ļ	0	5.6	0	3.0	0	4.8	0	0	15.4
9th	0	0	Ļ	5.0	8.2	0	7.8	0	0	0	0	(
10th	7.4	0	Ļ	0	5.4	0	8.8	0	0	0	0	(
11th	0	0	3.4 4 days	0	0	0	6.6	0	0	0	0	C
12th	0	0	0	0	0	2.6	0	0	3.6	0	0	5.0
13th	0	0	0	0	0	0	0	0	0	0	0	4.8
14th	0	0	0	0	0	0	0	0	13.2	5.8	0	4.0
15th	0	0	0	0	0	0	0	6.4	0	0	0	(
16th	11.0	0	0	13.2	12.8	0	0.4	Ļ	0	4.4	0	C
17th	0	0	0	4.0	1.6	0	5.0	Ļ	15.6	0	0	25.6
18th	0	3.2	0	8.4	3.4	4.6	6.0	7.4 3 days	0	0	0	(
19th	0	2.2	1.0	Ļ	5.4	6.8	0	0	0	9.8	0	(
20th	0	0	0	Ļ	0	8.6	0	0	0	0	0	(
21st	0	0	0	3.2 3 days	0	1.2	0	0	0	0	0	(
22nd	0	0	0	0	2.0	0.8	0	0.6	0	0	0	(
23rd	0	0	0	0	0	1.8	12.6	0	0	33.4	0	(
24th	0	0	0	9.2	6.2	1.8	1.8	7.4	0	0	0	(
25th	0	0	0	1.2	0	0	12.2	0.4	0	1.4	0	(
26th	0	0	0	2.2	0	1.4	0	0	0	0	0	(
27th	0	0	0	0	0	0	0	0	0	0	0	(
28th	0	0	0	0.8	0	1.8	0.6	0	0	0	0	(
29th	0		0	0	0	0	0.4	2.2	0	0	0	(
30th	0		0	2.4	0	0	0	2.0	0	0	0	(
31st	0		0		0		0	3.4		0		(
Highest Daily	11.0	3.2	1.0	13.2	14.8	8.6	12.6	7.4	15.6	33.4	0.0	25.6
Monthly Total	18.4	5.4	4.4	49.6	70.6	32.8	84.0	33.0	39.0	99.2	0.0	74.8

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	<b>25.0</b> 9th 1998	<b>30.8</b> 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

Gaps occur in the table where a valid observation is not available. This is frequently associated with the observer being unavailable (where observations are undertaken manually), a failure in the observing equipment, or when an event has produced suspect data.

Product Code: IDCJAC0009 reference: 33799372

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

Lat: 38.34° S	Lon: 144.3	1°E EI			Kev	/: Units = r	nm 12.3 =	Not quality	controlled	l. ⊥ = Part	of accumu	lated tot
1985	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	1.4	10.3	0	0	0	0	1.3	0	0	(
2nd	0	0	0	30.0	0	0	0	0	2.6	0	0	1.(
3rd	0	0	0	7.0	0	0	0	0	6.8	0	0	19.0
4th	0	0	2.2	0	0	19.4	0	0	2.0	0	0	(
5th	0	0	2.8	0	0	0	0	3.0	1.4	4.2	5.4	(
6th	5.0	3.0	2.6	0	0	0	0	0	0	0	9.6	(
7th	0	0	0	0	0	0	1.4	2.4	0	0	7.2	10.0
8th	0	0	0	0	11.4	0	0	2.0	0	0	0	6.0
9th	0	0	0	0	0	0	0	8.0	0	0	23.0	5.0
10th	0	0	0	0	0	0	0	4.0	0	0	0	6.4
11th	0	0	0	0	1.4	13.0	2.6	0	0	0	0	(
12th	0	0	0	0	0	0	0	0	0	0	0	(
13th	0	0	0	0	0	0	0	0	1.8	0	0	C
14th	0	0	0	Ļ	0	0	6.2	0	0	0	0	C
15th	0	0	0	21.0 2 days	4.6	1.0	3.2	1.6	0	0	8.0	C
16th	0	0	20.0	0	0	0	13.4	11.0	0	2.6	0	8.0
17th	0	0	6.4	2.2	0	0	3.8	5.0	0	9.0	5.4	(
18th	0	0	1.0	12.5	12.2	0	0	5.6	0	4.0	0	(
19th	0	0	0	17.5	0	0	0	4.2	2.0	1.2	0	(
20th	0	0	0	0	0	12.4	0	3.6	0	0	0	(
21st	0	0	0	0	0	1.2	7.4	0	0	0	2.4	C
22nd	0	0	0	0	1.5	11.6	7.0	0	0	3.8	0	4.0
23rd	0	0	0	0	0	3.4	0	12.6	0	0	0	2.0
24th	0	Ļ	1.2	0	0	0	0	0	0	28.6	0	C
25th	0	3.4 2 days	0	0	0	0	2.8	0	0	0	1.0	C
26th	0	1.4	0	0	0	0	0	8.4	5.8	0	0	(
27th	0	1.8	0	0	0	1.5	0	1.8	3.2	0	1.0	(
28th	0	0	0	0	17.0	1.8	4.4	8.2	0	0	0	(
29th	0		0	0	0	0	1.4	0	0	0	0	(
30th	0		0	0	2.4	0	7.0	1.2	0	4.0	0	(
31st	0		0		0		2.0	0		4.4		(
Highest Daily	5.0	3.0	20.0	30.0	17.0	19.4	13.4	12.6	6.8	28.6	23.0	19.0
Monthly Total	5.0	9.6	37.6	100.5	50.5	65.3	62.6	82.6	26.9	61.8	63.0	61.4

Annual total for 1985 = 626.8 mm

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	<b>42.0</b> 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	<b>30.8</b> 10th 1981	<b>39.2</b> 31st 2005	35.8 22nd 1976	40.4 3rd 1981	<b>45.0</b> 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

Gaps occur in the table where a valid observation is not available. This is frequently associated with the observer being unavailable (where observations are undertaken manually), a failure in the observing equipment, or when an event has produced suspect data.
Product Code: IDCJAC0009 reference: 33799365

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

					Key	: Units = r	nm 12.3 =	Not quality	controlled	I. ↓ = Part	of accumu	lated tot
1984	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	Ļ	0	0	0	0	3.0	0	0	0	4.0	0	C
2nd	17.8 2 days	0	0	0	0	0	0	0	Ļ	14.0	0	C
3rd	0	0	0	0	0	0	5.8	0	2.6 2 days	0	0	C
4th	0	0	0	0	0	0	3.0	0	9.4	0	0	(
5th	0	0	0	0	12.8	0	0	Ļ	0	0	0	(
6th	0	0	0	0	Ļ	0	0	16.4 2 days	0	0	0	15.2
7th	0	0	0	0	5.2 2 days	0	10.2	2 uays 0	0	0	0	C
8th	0	0	0	0	0	0	6.0	0	0	0	0	C
9th	0	0	0	0	0	0	0	0	0	0	0	C
10th	0	0	0	0	0	0	0	6.4	0	9.4	0	C
11th	0	0	0	0	0	0	0	0	0	5.4	14.0	C
12th	0	0	0	0	4.6	0	4.2	0	0	0	4.0	C
13th	0	0	6.4	0	0	0	0	0	0	0	0	C
14th	0	0	Ļ	0	0	0	0	0	2.2	0	0	(
15th	Ļ	0	Ļ	Ļ	0	0	Ļ	4.0	0	0	0	C
16th	23.2 2 days	0	7.0 3 days	<b>4.8</b> 2 days	0	0	15.4 2 days	0	Ļ	0	0	12.2
17th	0	0	0	0	0	Ļ	1.0	0	16.4 2 days	0	0	C
18th	0	0	0	0	0	3.2 2 days	0	0	9.2	0	0	(
19th	0	0	0	0	0	3.8	0	0	29.2	0	0	0
20th	0	0	0	15.2	0	0	0	0	3.8	0	0	12.2
21st	0	35.6	0	0	0	0	0	30.0	0	0	0	C
22nd	0	0	0	Ļ	5.6	0	Ļ	4.6	0	0	0	C
23rd	0	0	0	<b>7.6</b> 2 days	0	0	11.4 2 days	0	Ļ	0	0	C
24th	6.8	0	0	0	0	0	11.4	0	11.4 2 days	0	0	(
25th	0	0	Ļ	0	0	0	0	0	1.2	0	0	C
26th	0	0	28.8	0	0	0	0	10.2	0	0	0	C
27th	12.6	0	2 days 19.4	0	0	1.2	6.4	0	0	0	0	(
28th	0	7.4	4.6	0	0	4.6	0	3.0	3.6	0	0	(
29th	0	0	0	0	0	0	0	3.8	Ļ	0	0	C
30th	0		0	0	0	0	0	0	1.0 2 days	0	0	C
31st	0		0		0		0	0	2 00,0	0		C
Highest Daily	12.6	35.6	19.4	15.2	12.8	4.6	11.4	30.0	29.2	14.0	14.0	15.2
Monthly Total	60.4	43.0	66.2	27.6	28.2	15.8	74.8	78.4	90.0	32.8	18.0	39.6

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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Product Code: IDCJAC0009 reference: 33799358

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					Key	: Units = n	nm 12.3 =	Not quality	controlled	l. ↓ = Part	of accumu	lated tota
1983	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	Ļ	0	3.8	0	0	0	0	0
2nd	0	0	0	0	6.4 2 days	0	2.2	3.2	0	0	0	0
3rd	0	0	0.2	0	∠ days	0	0	0	1.8	0	2.6	0
4th	0	0	0	0	33.8	0	0	0	0	2.2	0	0
5th	0	0	10.4	0	2 days 0	0	0	0	0	0	0	C
6th	0	0	0	12.4	0	0	0	0	9.8	0	0	C
7th	0	0	0	0	0	0	Ļ	0	10.4	0	0	0
8th	0	0	2.8	0	0	Ļ	<b>17.4</b> 2 days	0	Ļ	0	0	0
9th	0	0	0	Ļ	0	Ļ	0	Ļ	<b>17.4</b> 2 days	0	0	0
10th	0	0	0	Ļ	0	12.8	0	6.2	2 days	0	0	0
11th	1.8	0	0	9.4	0	3 days 7.0	0	2 days 0	Ļ	0	0	0
12th	0	0	0	3 days 0	0	0	0	0	2.2	0	0	0
13th	0	0	0	2.0	0	0	0	0	2 days 0	Ļ	Ļ	0
14th	3.4	0	0	Ļ	0	0	0	0	30.2	10.8	6.6 2 days	0
15th	0	0	0	5.0	0	4.6	0	0	0	2 days 26.8	2 days	0
16th	0	0	1.6	2 days 1.2	0	0	0	0	0	Ļ	2.6	0
17th	0	0	0	0	0	0	0	9.4	0	<b>19.2</b> 2 days	0	0
18th	0	0	0	0	0	0	0	0	0	2 days	0	0
19th	0	0	0	0	0	0	0	0	0	0	0	0
20th	0	0	0	0	0	0	7.2	0	0	0	0	C
21st	0	0	0	0	Ļ	0	Ļ	0	6.2	0	0	0
22nd	0	0	18.4	0	13.4 2 days	0	<b>2.8</b> 2 days	0	0	0	0	0
23rd	0	0	12.0	Ļ	0	0	0	0	0	0	2.2	0
24th	0	0	Ļ	Ļ	0	0	0	Ļ	0	0	0	0
25th	0	0	<b>5.2</b> 2 days	Ļ	0	Ļ	0	Ļ	0	0	0	0
26th	0	0	2 uays 0	14.0 4 days	0	Ļ	0	Ļ	0	9.6	0	0
27th	0	0	0	4 days	0	16.6	5.8	16.2	0	0	0	C
28th	11.4	0	0	0	0	3 days 0	0	4 days 0	15.6	0	0	C
29th	0		0	0	0	3.8	Ļ	0	0	0	0	C
30th	0		0	0	0	18.4	16.4 2 days	0	0	0	0	C
31st	0		0		7.6		2 days	3.4		0		C
Highest Daily	11.4	0.0	18.4	12.4	7.6	18.4	7.2	9.4	30.2	26.8	2.6	0.0
Monthly Total	16.6	0.0	50.6	44.0	61.2	63.2	55.6	38.4	100.8	68.6	14.0	0.0

Annual total for 1983 = 513.0 mm

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

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					Key	r: Units = r	mm 12.3 =	Not quality	/ controlled	l. ↓ = Part	of accumu	lated tot
1982	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	0	0	0	0	0	0	0	0	(
2nd	0	0	0	0	0	0	0	0	0	0	0	(
3rd	0	0	0	0	0	0	2.2	0	10.6	Ļ	0	(
4th	3.0	0	0	0	0	0	0	0	2.6	2.6 2 days	0	C
5th	0	0	0	0	2.6	0	0	0	0	0	0	(
6th	0	0	Ļ	0	Ļ	0	0	0	0	0	0	(
7th	0	0	Ļ	0	4.0 2 days	0	5.2	0	3.4	0	0	2.6
8th	0	0	9.0 3 days	0	0	24.0	0	0	0.4	0	0	30.2
9th	0	0	0 dajo	0	0	0	0	0	Ļ	0	0	1
10th	0	0	0	0	0	Ļ	0	0	<b>8.8</b> 2 days	0	0	7.4 2 days
11th	0	0	0	0	0	<b>4.6</b> 2 days	Ļ	3.8	1.0	0	Ļ	(
12th	0	0	0	0	0	0	<b>2.8</b> 2 days	Ļ	0	0	1.0 2 days	(
13th	0	0	0	0	0	0	2 days 3.6	<b>4.8</b> 2 days	0	0	0	(
14th	0	0	0	0	0	0	0	0	0	0	0	(
15th	0	0	0	0	0	0	0	0	0	0	0	C
16th	0	0	0	0.8	0	0	0	0	0	0	6.8	(
17th	0	0	3.0	0	0	0	Ļ	0	0.4	Ļ	0	(
18th	0	0	0	0	0	0	Ļ	0	1.0	<b>8.4</b> 2 days	0	C
19th	0	0	0	0	4.2	Ļ	6.0 3 days	0	Ļ	0	0	C
20th	0	0	0	0	Ļ	Ļ	0	0	<b>2.2</b> 2 days	4.8	0	(
21st	0	0	0	0	<b>8.8</b> 2 days	5.0 3 days	0	0	0	0	0	(
22nd	0	0	0	0	4.8	5.4	0	0	0	3.4	0	(
23rd	0	0	8.2	0	0	0	0	0	0	0	0	(
24th	0	0	0	0	0	0	0	0	0	0	0	C
25th	6.4	0	0	Ļ	0	0	0	0	0	0	0	C
26th	11.0	0	0	<b>4.4</b> 2 days	0	0	0	0	Ļ	0	0	C
27th	0	0	Ļ	0.8	0	0	0	0	3.2 2 days	0	0	(
28th	0	0	Ļ	27.2	0	0	0	0	0	0	0	(
29th	0		23.0 3 days	0	0	0	Ļ	0	9.8	0	0	(
30th	0		0 000	0	Ļ	0	5.0 2 days	0	0	0	0.6	3.6
31st	0		0		21.8 2 days		2 days	0		0		(
Highest Daily	11.0	0.0	8.2	27.2	2 days	24.0	5.2	3.8	10.6	4.8	6.8	30.2
Monthly Total	20.4	0.0	43.2	33.2	46.2	39.0	24.8	8.6	43.4	19.2	8.4	43.8

#### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

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Product Code: IDCJAC0009 reference: 33799355

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

Lat: 38.34° S	Lon: 144.31		evation:		10		10.5					
								Not quality				
1981	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	1	0.3	0	3.4	0	0	0	0	0	(
2nd	0.2	0	5.6 2 days	0	0	Ļ	0	0	0	0	0	(
3rd	0	0	0	0	0	3.2 2 days	0	0	0	40.4	0	C
4th	0	0	0	0	0	0	Ļ	6.2	0	0	3.2	C
5th	0	15.4	0	Ļ	Ļ	0	Ļ	0	0	0	0	(
6th	0	0	0	<b>22.2</b> 2 days	Ļ	0	Ļ	0	0	0	0	C
7th	0	0	0	0	Ļ	Ļ	20.2 4 days	0	0	0	0	C
8th	0	Ļ	0	0	Ļ	Ļ	0	0	0	0	0	(
9th	5.0	0.6 2 days	0	0	Ļ	Ļ	0	Ļ	0	0	0	0
10th	18.4	0	4.0	0	Ļ	25.0 4 days	30.8	<b>10.8</b> 2 days	0	0	12.0	C
11th	0	0	0	0	Ļ	0	0	0	0.2	0	0	C
12th	0	0	0	Ļ	Ļ	0	0	5.2	0	0	Ļ	4.4
13th	0	0	0	3.0 2 days	Ļ	0	0	0	0	0	7.0 2 days	ļ
14th	0	0	0	0	Ļ	0	0	0	0	0	Ļ	9.6 2 days
15th	0	0	0	0	Ļ	0	1.8	3.2	0	0	Ļ	C
16th	2.6	0	0	0	Ļ	16.6	0	0	0	0	0.4 3 days	0
17th	0	0	0	0	Ļ	Ļ	0	0	0	3.0	0	C
18th	Ļ	0	0	0	Ļ	Ļ	0	0	0	0	0	C
19th	6.4 2 days	0	0	0	Ļ	Ļ	0	0	0	0	0	C
20th	0	0	0	0	Ļ	Ļ	Ļ	0	0	0	4.8	C
21st	0	0	2.2	0	Ļ	Ļ	Ļ	27.0	0	5.4	0	C
22nd	0	0	0	0	Ļ	Ļ	15.6 3 days	3.2	0	0	0	C
23rd	0	0	0	0	Ļ	Ļ	0	0	0	0	0	C
24th	0	0	0	0	Ļ	19.2 8 days	0	0	0	0	1.0	C
25th	0	0	0	0	55.4 21 days	0	0	0	0	0	0	C
26th	0	0	0	0	13.4	0	0	0	0	0	0	C
27th	Ļ	0	0	0	0	4.8	Ļ	Ļ	0	0	0	C
28th	33.0 2 days	0	23.6	0	0	11.4	Ļ	<b>20.4</b> 2 days	0	13.0	Ļ	C
29th	↓		0	5.2	Ļ	0	10.0 3 days	3.2	0	0	Ļ	C
30th	2.0 2 days		0	0	<b>4.2</b> 2 days	0	0	Ļ	0	0	16.4 3 days	C
31st	0		2.8		0		0	<b>4.4</b> 2 days		0		C
Highest Daily	18.4	15.4	23.6	5.2	13.4	16.6	30.8	27.0	0.2	40.4	12.0	4.4
Monthly Total	67.6	16.0	38.2	30.7	73.0	83.6	78.4	83.6	0.2	61.8	44.8	14.0

#### Annual total for 1981 = 591.9 mm

## Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

Gaps occur in the table where a valid observation is not available. This is frequently associated with the observer being unavailable (where observations are undertaken manually), a failure in the observing equipment, or when an event has produced suspect data.

Product Code: IDCJAC0009 reference: 33799351

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Page created: Mon 11 Dec 2017 06:12:50 AM EST

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Observations of Daily rainfall are nominally made at 9 am local clock time and record the total for the previous 24 hours. Rainfall includes all forms of precipitation that reach the ground, such as rain, drizzle, hail and snow. About rainfall data

					Key	: Units = r	nm 12.3 =	Not quality	controlled	. ↓ = Part	of accumu	lated tot
1978	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	5.8	0	0	0	0	7.0	0	0	(
2nd	0	0	0	5.6	0	1.8	0	0	0	0	0	(
3rd	0	0	0	0	0	7.4	17.2	0	4.2	2.6	0	(
4th	0	0	0	0	0	10.4	0.8	0	0	0	0	15.6
5th	0	0	0	0	0	0	1.2	0	0	0	0	4.2
6th	0	3.0	0	0	0	0	14.8	0	0	0	27.2	C
7th	0	0.4	0	0	8.6	0	1.8	27.4	1.6	0	0	C
8th	0	0	0	0	0	1.4	0	9.2	0	0	0	(
9th	0	1.4	0	0	0	0	0	15.0	0	0	0	C
10th	0	0	0	27.8	4.4	4.6	0	5.8	0	0	0	(
11th	0	9.2	0	3.2	7.0	0	0	0	0	0	28.6	(
12th	0	0	0	2.8	0	4.2	8.2	3.6	23.4	0	0	17.2
13th	0	1.0	14.8	0	14.4	0	0	9.2	8.4	2.8	0	31.0
14th	0	0	0	0	Ļ	0	0	0.2	14.6	0	0	1.2
15th	0	0	0	0	3.4 2 days	0	Ļ	0.4	0.6	0	0	C
16th	0	0	0	0	0	0	Ļ	0	0	0	0	(
17th	0	0	0	0	12.6	0	5.0 3 days	1.2	0	0	0	29.4
18th	0	0	0	0	6.0	6.0	0	0	7.6	12.6	0	4.0
19th	0	0	0	0	0	1.4	2.8	0	3.4	0.6	Ļ	(
20th	0	0	0	0	6.4	0	11.6	0	0	0	58.6 2 days	C
21st	0	0	3.8	0	0	0	0	0	0	0	0	(
22nd	0	0.6	0.2	0	0	0	Ļ	2.0	0	0	0	(
23rd	0	0	12.8	0	3.4	0	Ļ	3.0	0	0	0	C
24th	3.8	0	0	0	0	1.8	9.2 3 days	0	0	0	0	C
25th	0	0	0	0	4.0	0	1.8	0	0	0	0	(
26th	0	0	2.4	0	0	0	0	0	0	16.6	0	20.2
27th	0	0	0	7.0	0	0	0	0	9.8	26.0	0	(
28th	0	5.4	0	0	0	0	5.8	0	0.2	0	0	(
29th	1.8		0	0	0	0	0	0	0	0	1.0	(
30th	15.2		4.2	0	12.2	0	0	0	0	0	0	(
31st	8.4		17.6		0		0	0		0		(
Highest Daily	15.2	9.2	17.6	27.8	14.4	10.4	17.2	27.4	23.4	26.0	28.6	31.0
Monthly Total	29.2	21.0	55.8	52.2	82.4	39.0	80.2	77.0	80.8	61.2	115.4	122.8

### Summary statistics for all years

Statistic	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest Daily	42.0 1st 1988	90.0 8th 2002	56.0 22nd 2001	70.0 23rd 2001	38.6 6th 1977	25.0 9th 1998	30.8 10th 1981	39.2 31st 2005	35.8 22nd 1976	40.4 3rd 1981	45.0 22nd 1988	61.2 2nd 1987

Data within the table which are in italics represent observations which have not been fully quality controlled, a process which may take a number of months to complete. While these data may be correct, you should exercise caution in their use. For observations of daily rainfall which span more than one day it indicates that there is some uncertainty associated with the exact date on which the daily rainfall occurred.

Gaps occur in the table where a valid observation is not available. This is frequently associated with the observer being unavailable (where observations are undertaken manually), a failure in the observing equipment, or when an event has produced suspect data.

Product Code: IDCJAC0009 reference: 33799342

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Page created: Mon 11 Dec 2017 06:11:22 AM EST

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# TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

1977	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	3.2	0	0	0	3.4	17.2	0.2	1.0	0	0	0	0
2nd	0	0	0	0	0	4.6	0	0	0	25.8	0	0
3rd	0.4	0	0	0	0	1.0	0	0	5.4	0	0	0
4th	0	0	0	0	0	0	0	5.8	5.0	0	2.0	0
5th	0	0	0	0	0	0	0	0	0	3.0	0	0
6th	0	0	0	0	38.6	0	0	0	0	7.0	0	0
7th	0	0	0	0	0	0	0	0	0	0	0	0
8th	0	0.8	0	4.2	0	8.0	0	1.2	0	0	0	0
9th	0	0	0	0	0.4	2.4	0	0	0	0	0	0
10th	0	0	0	0	0	0	0	0	7.2	0	22.0	0
11th	0	0	0	0	5.0	8.8	1.0	0	0	0	0	0
12th	0	0	0	0	2.8	1.2	0	1.0	0	0	0	0
13th	0	14.0	0	0	0.2	0	0	1.6	10.2	0	0	0
14th	1.2	0	0	0	0	0	12.6	0	0.8	0.6	3.0	0
15th	13.2	0	0	0	0	1.6	6.4	0	5.0	0	0	0
16th	5.2	0	8.4	0	0	3.2	0.4	1.8	1.2	0	0	0
17th	20.4	0	0	0	0	1.8	0	0	0	0	0	0
18th	3.2	3.2	0	0	2.4	24.4	0	0	0	0	0	0
19th	0	0	0	0.2	0	12.2	0	0	0	5.0	0	0.4
20th	0	0	0	0	1.8	0.8	0	0	0	0	0	0
21st	0	0	0	0	0	2.2	0	5.0	0	0	0	0
22nd	0	0	0	0	0	0	0	8.8	0	0	0	0
23rd	0	0	0	0	10.6	1.6	0.2	0	0	0	0	0
24th	0	23.8	1.6	0	6.4	8.2	0	0	0	0	0	0
25th	0	0	0	0	0.6	0	6.6	0	0	0	0	0
26th	0	0	11.2	0	0.2	0	14.8	0	0	0	0	2.8
27th	0	0	3.8	0	0	0	1.8	0	0	0	0	2.0
28th	0	1.4	0	0	0	7.6	1.2	0	0	5.6	9.2	5.2
29th	0		0	3.4	0	13.2	0	0	0	0	0	1.4
30th	0		1.4	0	6.2	7.4	4.0	0	0	0	0	0
31st	0		0		9.8		0	3.6		0		0
Highest daily	20.4	23.8	11.2	4.2	38.6	24.4	14.8	8.8	10.2	25.8	22.0	5.2
Monthly Total	46.8	43.2	26.4	7.8	88.4	127.4	49.2	29.8	34.8	47.0	36.2	11.8

Annual total for 1977 = 548.8mm

 $\downarrow$  This day is part of an accumulated total Quality control: 12.3 Done & acceptable, *12.3* Not completed or unknown

Product code: IDCJAC0009 reference: 33779718



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# TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest daily	42.0	90.0	56.0	70.0	38.6	25.0	30.8	39.2	35.8	40.4	45.0	61.2
Date of highest daily	1st 1988	8th 2002		23rd 2001	6th 1977	9th 1998	10th 1981	31st 2005	22nd 1976	3rd 1981	22nd 1988	2nd 1987

## Statistics for this station calculated over all years of data

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.



Product code: IDCJAC0009 reference: 33779718 Created on Sat 09 Dec 2017 20:08:56 PM EST

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# TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

1976	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	18.2	0	0	0	0	0	3.4	0	0	1.4
2nd	0	0	0	0	0	5.8	0	15.0	5.2	0	8.8	0
3rd	0	0	0	0	0	0.2	0	1.6	0.4	9.2	19.4	0
4th	0	0	0	0	1.4	0.6	0	0	2.6	10.6	0.6	5.8
5th	2.2	0	0	1.4	1.0	0	2.2	0	0	0.2	0	0
6th	0	0	0	0	1.4	0	1.4	1.8	0	4.2	0	0
7th	0	0	0	0	5.0	6.0	0.2	$\downarrow$	0	2.0	0	0.4
8th	0	0	0	0	2.2	0.2	0	$\downarrow$	0	7.4	0	0
9th	0	3.8	0	2.0	0	0	0	7.2	9.8	6.6	2.8	0
10th	0	0	0	0	0	0.2	0	1.8	6.0	0.3	0	0
11th	0	0	0	0	0	0	0	8.8	1.6	0	0	0
12th	0	0	0	0	0	0	1.2	4.4	0.8	0	1.8	4.2
13th	2.6	0	0	0	0	0	0	9.6	2.0	0	0	1.6
14th	0	0	0	0	0	0	0	0	1.6	3.8	0	0
15th	1.0	0	0	12.8	0	0	2.2	0	0	4.4	0	11.6
16th	0	0	0	0	3.4	4.6	0	0	0	13.8	10.8	3.4
17th	0	0	11.0	0	1.8	4.2	0	0	0.6	0.6	3.4	2.6
18th	0	0	0	0	0	0	0	0.2	0	0	2.6	0
19th	0	4.2	0	0	0.4	0	0	0	0	0	1.4	0
20th	0	0	0	0	0	0	0	0	4.2	0	0	0
21st	0	0	0	0	0	0	0	0	18.4	0	0	0
22nd	0	0	0	0	2.8	0	0	0	35.8	0	0	0
23rd	0	0	0	0	1.2	0	0	8.6	14.4	5.0	0	1.2
24th	0	0	0	0	0	0	0	9.8	0	0	0	8.4
25th	1.2	0	0	0	0	0	0	0	0	0	2.6	0
26th	1.4	0	0	0	2.6	0	0	0	0	0	0	0
27th	0	0	0	0	0	0	0.4	0	0	0	0	0
28th	0	0	2.2	0	0	10.6	0	0	0	0	0	0
29th	0	0.6	0.8	5.4	0	4.8	2.4	0	3.4	0	0	0
30th	0		0	0.6	0	0	1.2	1.2	0	0	10.6	0
31st	0		0		0		0	0		0		0
Highest daily	2.6	4.2	18.2	12.8	5.0	10.6	2.4	15.0	35.8	13.8	19.4	11.6
Monthly Total	8.4	8.6	32.2	22.2	23.2	37.2	11.2	70.0	110.2	68.1	64.8	40.6

Annual total for 1976 = 496.7mm

 $\downarrow$  This day is part of an accumulated total

Quality control: 12.3 Done & acceptable, 12.3 Not completed or unknown

Product code: IDCJAC0009 reference: 33779697



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# TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest daily	42.0	90.0	56.0	70.0	38.6	25.0	30.8	39.2	35.8	40.4	45.0	61.2
Date of highest daily	1st 1988	8th 2002		23rd 2001	6th 1977	9th 1998	10th 1981		22nd 1976	3rd 1981	22nd 1988	2nd 1987

## Statistics for this station calculated over all years of data

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.



Product code: IDCJAC0009 reference: 33779697 Created on Sat 09 Dec 2017 20:08:24 PM EST

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## Daily Rainfall (millimetres)

## TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

1975	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1st	0	0	0	2.8	0	1.6	0	0.1	0	0	2.8	0
2nd	0	0	0	0	0	0	0	0.2	0	2.0	0	0
3rd	0	0	3.4	0.2	0	0	0	9.0	18.6	9.8	1.2	0.4
4th	0	0	0	0	0	1.6	0	0	3.6	1.4	8.4	7.6
5th	0	0	0	2.0	2.2	7.4	2.0	1.6	0.8	0	2.6	0
6th	0	0	0	0.1	0.4	7.6	2.0	1.0	0.2	0	8.6	0
7th	0	0	4.2	0	2.6	0	3.0	0.8	0.2	0	2.2	0
8th	0	0	0	0	1.6	0	0	0	0	16.0	0	0
9th	4.2	0	0.6	0	0	0	0	0	0	6.4	0	0
10th	2.4	0	0	0	2.4	0	0.8	0	0	4.2	0.4	0
11th	8.0	0	2.2	0.2	0	2.6	0	9.8	0	5.8	0	0
12th	0	0	0	0	2.6	2.4	5.8	6.6	0	5.8	0.4	0.4
13th	1.1	0.1	0	0	0	2.0	0.4	2.6	20.6	5.0	0	0.2
14th	0	0	0	0	6.8	0	6.8	0.6	0.6	1.0	0	3.8
15th	0	0	11.2	0	2.8	0	1.1	1.0	0	0	0	0
16th	0	0	10.4	0	0	0	0	0	8.8	4.6	0	0
17th	0	0	0	0	0	0	0	0	5.0	0.6	0	0
18th	0	0	0	0	6.8	0	0.2	0.4	8.8	0	0	3.8
19th	0	0	14.9	0	1.8	0	1.0	3.2	1.4	0	0	0
20th	0	0	2.9	0	0	0	4.2	0	0	6.0	2.4	0
21st	0	0	1.2	0	0	0	0	5.0	1.2	9.4	11.6	0
22nd	0	0	0	0	0	0	0	1.2	5.2	0	0	0
23rd	0	0	0	0	0	0	0	9.4	1.6	0	0	0
24th	0	0	2.4	0	1.2	0	0.8	1.2	0	14.2	15.8	0
25th	0.4	0	0	2.0	0	0	0.6	1.0	0	0	0.6	0
26th	0.8	0	0	0	0	0	0	3.0	0	11.0	3.0	0
27th	0	6.6	0	0	4.8	0.2	0	9.0	0	0	0	0
28th	0	0	0	1.2	0	0	0	7.8	13.2	0	0	0
29th	0		0	1.2	0	1.8	8.4	0.8	0	0	0	2.2
30th	0		2.8	0	0	0	0	0.2	0.2	7.8	0	6.0
31st	0		2.4		0		11.0	0		22.2		0
Highest daily	8.0	6.6	14.9	2.8	6.8	7.6	11.0	9.8	20.6	22.2	15.8	7.6
Monthly Total	16.9	6.7	58.6	9.7	36.0	27.2	48.1	75.5	90.0	133.2	60.0	24.4

Annual total for 1975 = 586.3mm

 $\downarrow$  This day is part of an accumulated total Quality control: 12.3 Done & acceptable, *12.3* Not completed or unknown

Product code: IDCJAC0009 reference: 33779678



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## Daily Rainfall (millimetres)

### TORQUAY GOLF CLUB

Station Number: 087160 · State: VIC · Opened: 1974 · Status: Open · Latitude: 38.34°S · Longitude: 144.31°E · Elevation: 15 m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Mean	33.6	27.1	37.6	39.1	53.2	50.8	57.6	58.3	52.5	55.9	45.7	41.2
Median	28.9	16.0	32.2	32.0	52.2	47.0	54.0	64.0	43.4	50.9	37.0	39.6
Highest daily	42.0	90.0	56.0	70.0	38.6	25.0	30.8	39.2	35.8	40.4	45.0	61.2
Date of highest daily	1st 1988	8th 2002		23rd 2001	6th 1977	9th 1998	10th 1981		22nd 1976	3rd 1981	22nd 1988	2nd 1987

### Statistics for this station calculated over all years of data

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.

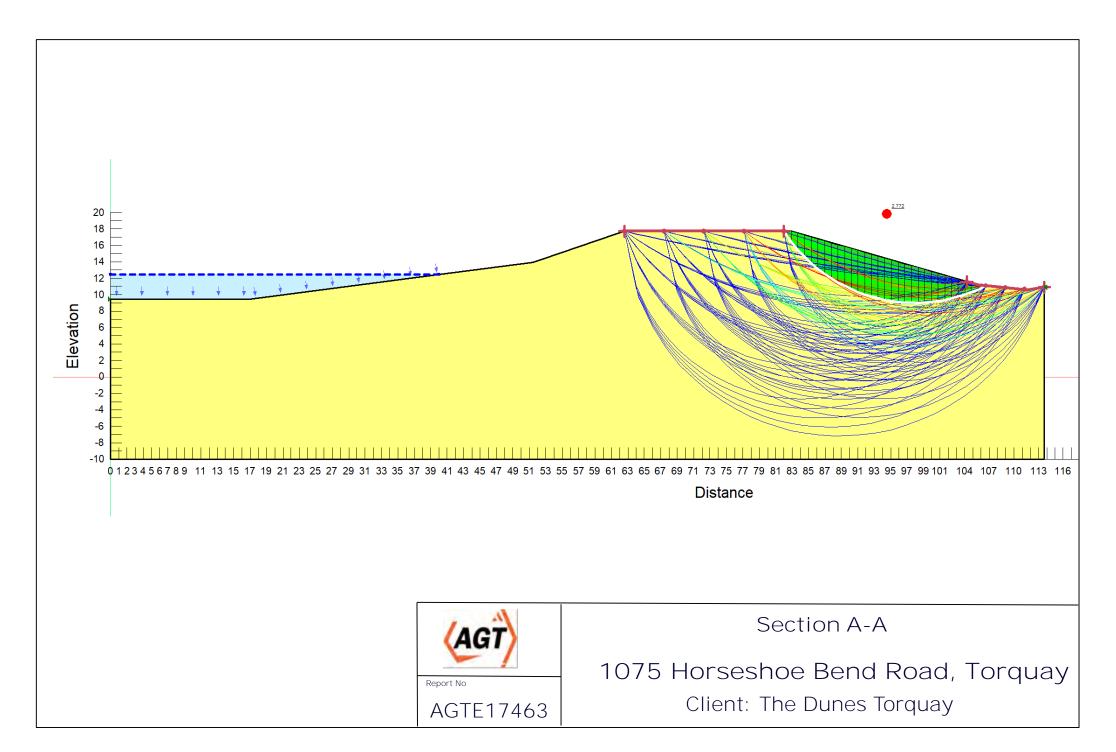


Product code: IDCJAC0009 reference: 33779678 Created on Sat 09 Dec 2017 20:07:56 PM EST

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# Appendix E – Slope/W Analysis



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 12 Date: 10/12/2017 Time: 04:48:01 PM Tool Version: 9.0.2.15352 File Name: Torquay Section A-A.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 04:51:49 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (62.582, 17.72) m Left-Zone Right Coordinate: (81.98522, 17.69133) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (104.28865, 11.5693) m Right-Zone Right Coordinate: (113.706, 10.9) m Right-Zone Increment: 4 Radius Increments: 4

## **Slip Surface Limits**

Left Coordinate: (0, 9.45) m Right Coordinate: (113.706, 10.9) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	12.45 m
Coordinate 2	40 m	12.45 m

	Х	Y
Point 1	40 m	12.45 m

Point	51.455	13.94
2	m	m
Point	62.582	17.72
3	m	m
Point	82.885	17.69
4	m	m
Point	105.65	11.18
5	m	m
Point	111.706	10.6
6	m	m
Point	113.706	10.9
7	m	m
Point	113.706	-10 m
8	m	-10 111
Point	0 m	-10 m
9	UIII	-10 111
Point	0 m	9.45
10	UIII	m
Point	16.936	9.45
11	m	m

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	2,652.5 m <sup>2</sup>

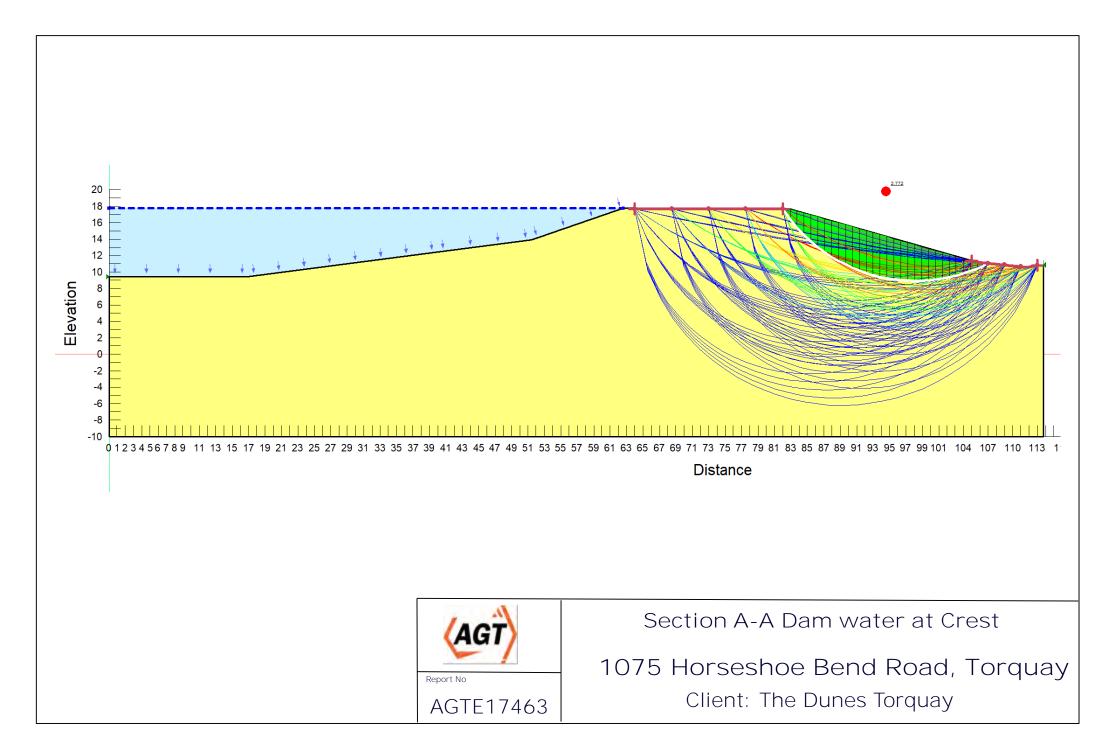
## **Current Slip Surface**

Slip Surface: 108 Factor of Safety: 2.772 Volume: 86.264875 m<sup>3</sup> Weight: 1,725.2975 kN Resisting Moment: 21,061.32 kN·m Activating Moment: 7,596.7759 kN·m Resisting Force: 1,011.0572 kN Activating Force: 364.67802 kN Slip Rank: 1 of 125 slip surfaces Exit: (106.61019, 11.08804) m Entry: (81.98522, 17.69133) m Radius: 19.06101 m Center: (97.968109, 28.077347) m

	х	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	82.43511 m	17.057205 m	0 kPa	6.0320123 kPa	2.8127735 kPa	10 kPa
Slice 2	83.291518 m	15.931846 m	0 kPa	22.572139 kPa	10.525561 kPa	10 kPa
Slice 3	84.104554 m	15.009345 m	0 kPa	33.775957 kPa	15.749987 kPa	10 kPa

Slice	84.917589	14.195895	0	43.245522	20.165718	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	85.730625	13.473074	0	51.404979	23.970535	
5	m	m	kPa	kPa	kPa	10 kPa
Slice	86.543661	12.827886	0	58.550258	27.302433	
6	m	m	kPa	kPa	kPa	10 kPa
Slice	87.356696	12.250772	0	64.891357	30.259337	
7	m	m	kPa	kPa	kPa	10 kPa
Slice	88.169732	11.734482	0	70.576659	32.910437	
8	m	m	kPa	kPa	kPa	10 kPa
Slice	88.982768	11.273382	0	75.707651	35.303057	
9	m	m	kPa	kPa	kPa	10 kPa
Slice	89.795804	10.863021	0	80.348158	37.466961	
10	m	m	kPa	kPa	kPa	10 kPa
Slice	90.608839	10.499832	0	84.530314	39.417133	
11	m	m	kPa	kPa	kPa	10 kPa
		1				
Slice	91.421875	10.180936	0	88.258559	41.155642	10 kPa
12	m	m	kPa	kPa	kPa	
Slice	92.234911	9.9039922	0	91.512518	42.672988	10 kPa
13	m	m	kPa	kPa	kPa	
Slice	93.047946	9.6671044	0	94.249359	43.949198	10 kPa
14	m	m	kPa	kPa	kPa	
Slice	93.860982	9.468739	0	96.406131	44.954917	10 kPa
15	m	m	kPa	kPa	kPa	IUKFa
Slice	94.674018	9.3076718	0	97.902476	45.652674	10 10
16	m	m	kPa	kPa	kPa	10 kPa
Slice	95.487054	9.1829471	0	98.644064	45.998483	1010
17	m	m	kPa	kPa	kPa	10 kPa
Slice	96.300089	9.0938472	0	98.527018	45.943903	
18	m	m	kPa		kPa	10 kPa
Slice	97.113125	9.0398708	0	97.443474	45.438638	
19	m	m	kPa	kPa	kPa	10 kPa
Slice	97.926161	9.020719	0	95.288275	44.433652	
20	m	m	kPa	kPa	kPa	10 kPa
				кга		
Slice	98.739196	9.0362866	0	91.96657 kPa	42.884716	10 kPa
21	m	m	kPa		kPa	
Slice	99.552232	9.0866589	0	87.40186 kPa	40.756157	10 kPa
22	m	m	kPa		kPa	
Slice	100.36527	9.1721149	0	81.543779	38.024489	10 kPa
23	m	m	kPa	kPa	kPa	
Slice	101.1783	9.2931342	0	74.374732	34.681507	10 kPa
24	m	m	kPa	kPa	kPa	
Slice	101.99134	9.4504113	0	65.914405	30.736392	10 kPa
25	m	m	kPa	kPa	kPa	TO KPd
Slice	102.80437	9.6448762	0	56.221272	20.24.044.1.5	10 -
26	m	m	kPa	kPa	26.21641 kPa	10 kPa
Slice	103.61741	9.8777236	0	45.390484		
27	m	m	kPa	kPa	21.16593 kPa	10 kPa
21		10.150453	0		15.643671	
				I see a see a see	T T T T T T T T T T T T T T T T T T T	1
Slice 28	104.43045 m	m	kPa	33.54796 kPa	kPa	10 kPa

Slice	105.24348	10.46492	0	20.841008	9.7183216	
29	m	m	kPa	kPa	kPa	
Slice	106.13009	10.860443	0	8.1294925	3.7908446	10 kPa
30	m	m	kPa	kPa	kPa	



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 16 Date: 10/12/2017 Time: 04:47:40 PM Tool Version: 9.0.2.15352 File Name: Torquay Section A-A Water at top of Dam.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:49:09 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### Sandy Clay

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (64, 17.7179) m Left-Zone Right Coordinate: (82, 17.69131) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (105, 11.36588) m Right-Zone Right Coordinate: (113, 10.7941) m Right-Zone Increment: 4 Radius Increments: 4

# **Slip Surface Limits**

Left Coordinate: (0, 9.45) m Right Coordinate: (113.706, 10.9) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	17.72 m
Coordinate 2	62.582 m	17.72 m

	Х	Y
Point 1	40 m	12.45 m

Point	51.455	13.94
2	m	m
Point	62.582	17.72
3	m	m
Point	82.885	17.69
4	m	m
Point	105.65	11.18
5	m	m
Point	111.706	10.6
6	m	m
Point	113.706	10.9
7	m	m
Point	113.706	-10 m
8	m	-10 111
Point	0 m	-10 m
9	UIII	-10 111
Point	0 m	9.45
10	UIII	m
Point	16.936	9.45
11	m	m

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	2,652.5 m <sup>2</sup>

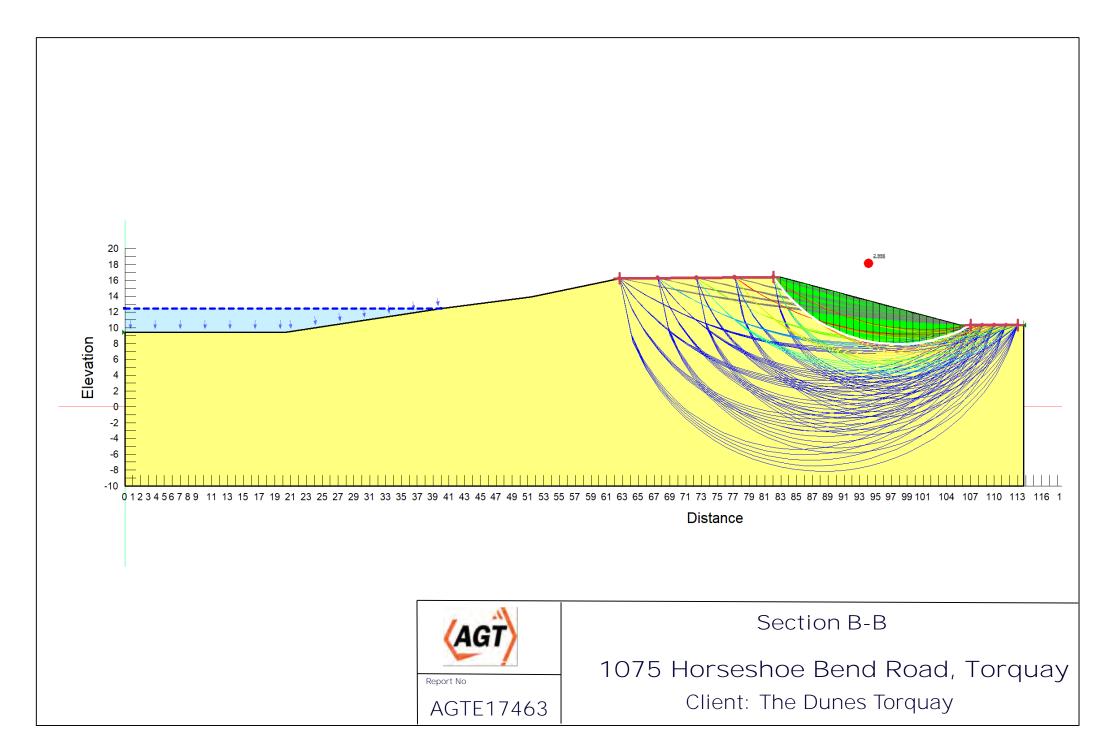
# **Current Slip Surface**

Slip Surface: 108 Factor of Safety: 2.772 Volume: 88.046528 m<sup>3</sup> Weight: 1,760.9306 kN Resisting Moment: 21,729.131 kN·m Activating Moment: 7,839.1083 kN·m Resisting Force: 1,030.6451 kN Activating Force: 371.81207 kN Slip Rank: 1 of 125 slip surfaces Exit: (106.9849, 11.052153) m Entry: (82, 17.691308) m Radius: 19.294269 m Center: (98.171157, 28.215684) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	82.4425 m	17.067024 m	0 kPa	5.8753863 kPa	2.7397376 kPa	10 kPa
Slice 2	83.306574 m	15.932566 m	0 kPa	22.496067 kPa	10.490088 kPa	10 kPa
Slice 3	84.149722 m	14.975929 m	0 kPa	34.121136 kPa	15.910947 kPa	10 kPa

Slice	84.99287	14.134911	0	43.908382	20.474815	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	85.836019	13.389612	0	52.314411	24.394611	1010
5	m	m	kPa	kPa	kPa	10 kPa
Slice	86.679167	12.726093	0	59.655353	27.817748	
6	m	m	kPa	kPa	kPa	10 kPa
Slice	87.522315	12.134163	0	66.153809	30.848028	
7	m	m	kPa	kPa	kPa	10 kPa
Slice	88.365463	11.606123	0	71.965582	33.558102	
8	m	m	kPa	kPa	kPa	10 kPa
Slice	89.208611	11.13602	0	77.195712	35.996952	
9	m	m	kPa	kPa	kPa	10 kPa
Slice	90.051759	10.719165	0	81.908475	38.194549	
10	m	m	kPa	kPa	kPa	10 kPa
Slice	90.894907	10.351816	0	86.133799		
11	m	m	kPa	kPa	40.16485 kPa	10 kPa
Slice	91.738056	10.030964	0	89.871569	41.907801	
12	m	m	kPa	kPa	kPa	10 kPa
Slice	92.581204	9.7541778	0			
13	m	m	kPa	93.09476 kPa	43.4108 kPa	10 kPa
Slice	93.424352	9.5194954	0	95.752088	44.649932	
14	m	m	kPa	kPa	kPa	10 kPa
Slice		9.3253438	0	Ki u	Ki u	
15	94.2675 m	m	kPa	97.77073 kPa	45.59124 kPa	10 kPa
Slice	95.110648	9.1704805	0	99.059581	46.192241	
16	95.110048 m	9.1704805 m	kPa	kPa	40.192241 kPa	10 kPa
			0	ΝΓα	NF d	
Slice 17	95.953796 m	9.053951 m	kPa	99.51342 kPa	46.40387 kPa	10 kPa
Slice			0	99.018277	46 172091	
511Ce 18	96.796944 m	8.9750574 m	kPa	kPa	46.172981 kPa	10 kPa
Slice 19	97.640093	8.9333368	0 kPa	97.458121 kPa	45.445468 kPa	10 kPa
	m	m			KFd	
Slice 20	98.483241	8.9285475	0	94.722784	44.16996 kPa	10 kPa
	m	m	kPa	kPa		
Slice	99.326389	8.9606619	0	90.716769	42.301924	10 kPa
21	m	m	kPa	kPa	kPa	
Slice	100.16954	9.0298656	0	85.368286	39.807885	10 kPa
22	m	m	kPa	kPa	kPa	
Slice	101.01269	9.1365631	0	78.637604	36.669317	10 kPa
23	m	m	kPa	kPa	kPa	
Slice	101.85583	9.2813895	0	70.52361 kPa	32.8857 kPa	10 kPa
24	m	m	kPa			
Slice	102.69898	9.4652302	0	61.06746 kPa	28.476224	10 kPa
25	m	m	kPa		kPa	
Slice	103.54213	9.689249	0	50.35239 kPa	23.479705	10 kPa
26	m	m	kPa	50.00200 Kr d	kPa	TOWN
Slice	104.38528	9.9549283	0	38.499202	17.952473	10 kPa
27	m	m	kPa	kPa	kPa	TO KEQ
Slice	105.22843	10.264122	0	25.657492	11.964285	10 kPc
20	m	m	kPa	kPa	kPa	10 kPa
28						

Slice	105.98372	10.577675	0	14.881522	6.9393675	
29	m	m	kPa	kPa	kPa	
Slice	106.65117	10.888824	0	6.3774621	2.9738594	10 kPa
30	m	m	kPa	kPa	kPa	



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 16 Date: 10/12/2017 Time: 04:47:04 PM Tool Version: 9.0.2.15352 File Name: Torquay Section B-B.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:31:52 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (62.582, 16.28) m Left-Zone Right Coordinate: (82.07605, 16.40482) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (107.02658, 10.35) m Right-Zone Right Coordinate: (113.02256, 10.35) m Right-Zone Increment: 4 Radius Increments: 4

## **Slip Surface Limits**

Left Coordinate: (0, 9.46) m Right Coordinate: (113.706, 10.35) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	12.46 m
Coordinate 2	40 m	12.46 m

	Х	Y
Point 1	40 m	12.46 m

Point	51.455	13.91
2	m	m
Point	62.582	16.28
3	m	m
Point	82.885	16.41
4	m	m
Point	105.65	10.35
5	m	m
Point	111.706	10.35
6	m	m
Point	113.706	10.35
7	m	m
Point	113.706	-10 m
8	m	-10 111
Point	0 m	-10 m
9	0	10
Point	0 m	9.46
10	- U III	m
Point	20.403	9.46
11	m	m

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	2,583.7 m <sup>2</sup>

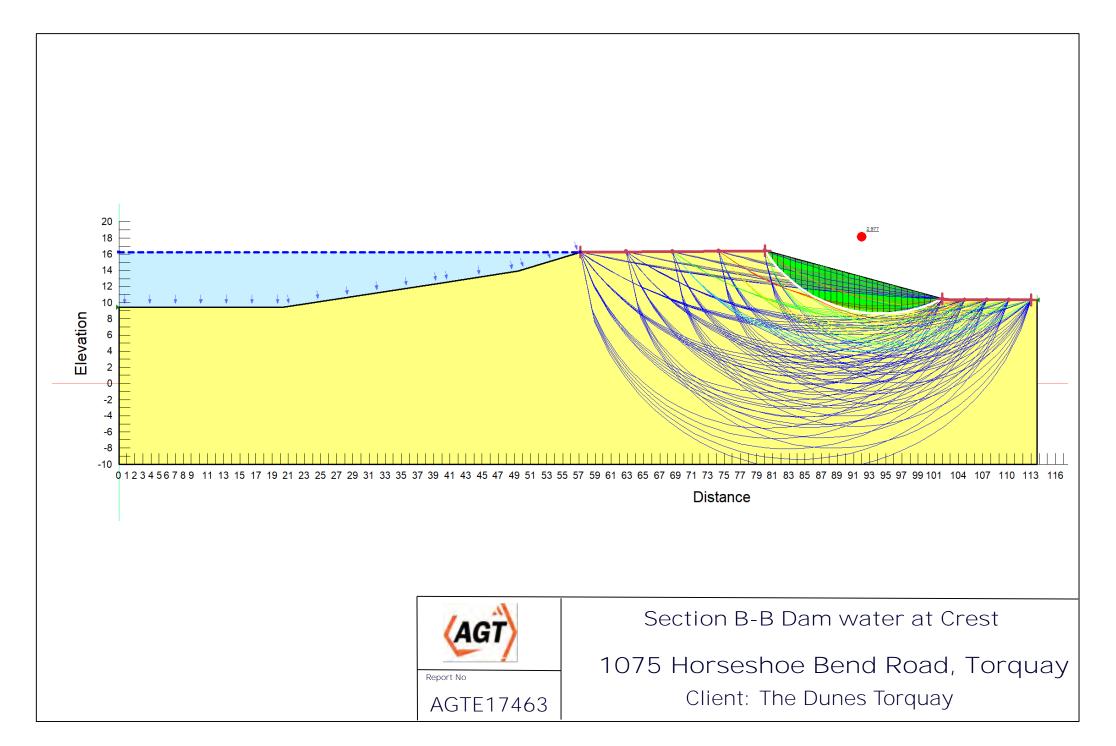
# **Current Slip Surface**

Slip Surface: 103 Factor of Safety: 2.998 Volume: 87.230107 m<sup>3</sup> Weight: 1,744.6021 kN Resisting Moment: 21,153.281 kN·m Activating Moment: 7,056.0959 kN·m Resisting Force: 1,028.7174 kN Activating Force: 343.1397 kN Slip Rank: 1 of 125 slip surfaces Exit: (107.02658, 10.35) m Entry: (82.07605, 16.40482) m Radius: 18.848878 m Center: (97.806111, 26.789682) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	82.480525 m	15.838766 m	0 kPa	5.4333012 kPa	2.5335899 kPa	10 kPa
Slice 2	83.306574 m	14.764396 m	0 kPa	21.508103 kPa	10.029393 kPa	10 kPa
Slice 3	84.149722 m	13.812445 m	0 kPa	33.520154 kPa	15.630705 kPa	10 kPa

Slice	84.99287	12.977718	0	43.623116	20.341793	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	85.836019	12.239801	0	52.285776	24.381258	
5	m	m	kPa	kPa	kPa	10 kPa
Slice	86.679167	11.584473	0	59.831927	27.900086	
6	m	m	kPa	kPa	kPa	10 kPa
Slice	87.522315	11.001377	0	66.489433	31.004532	
7	m	m	kPa	kPa	kPa	10 kPa
Slice	88.365463	10.482719	0	72.417995	33.769066	
8	m	m	kPa	kPa	kPa	10 kPa
Slice	89.208611	10.02249	0	77.725784	36.244128	
9	m	m	kPa	kPa	kPa	10 kPa
Slice	90.051759	9.615974	0	82.479819	38.460971	
10	m	m	kPa	kPa	kPa	10 kPa
Slice	90.894907	9.2594198	0		40.434792	
11	m	m	kPa	86.71269 kPa	kPa	10 kPa
Slice	91.738056	8.9498223	0	90.427105	42.166852	
12	91.758050 m	0.9490225 m	kPa	kPa	42.100852 kPa	10 kPa
Slice	92.581204	8.6847657	0	93.599236	43.646041	
13	92.581204 m	o.0647057 m	kPa	kPa	45.646041 kPa	10 kPa
Slice	93.424352		0			
511Ce 14		8.4623122 m	kPa	96.181538 kPa	44.850188 kPa	10 kPa
	m					
Slice 15	94.2675 m	8.2809222	0 kPa	98.105574 kPa	45.747381 kPa	10 kPa
	05 440640	m				
Slice	95.110648	8.1393945	0	99.285284	46.297488	10 kPa
16	m	m	kPa	kPa	kPa	
Slice	95.953796	8.0368248	0	99.621039	46.454053	10 kPa
17	m	m	kPa	kPa	kPa	
Slice	96.796944	7.9725747	0	99.004738	46.166667	10 kPa
18	m	m	kPa	kPa	kPa	
Slice	97.640093	7.9462513	0	97.326052	45.383883	10 kPa
19	m	m	kPa	kPa	kPa	
Slice	98.483241	7.9576953	0	94.479736	44.056624	10 kPa
20	m	m	kPa	kPa	kPa	10 10 0
Slice	99.326389	8.0069758	0	90.37369 kPa	42.141944	10 kPa
21	m	m	kPa	50.57505 Ki d	kPa	10 11 0
Slice	100.16954	8.0943928	0	84.937206	39.60687 kPa	10 kPa
22	m	m	kPa	kPa	55.00087 KFa	10 KF a
Slice	101.01269	8.2204859	0	78.128594	36.431962	10 kPa
23	m	m	kPa	kPa	kPa	TO KEQ
Slice	101.85583	8.3860518	0	69.941219	32.614126	10 kPa
24	m	m	kPa	kPa	kPa	TOKPO
Slice	102.69898	8.5921703	0	60.406969	28.168232	10 100
25	m	m	kPa	kPa	kPa	10 kPa
Slice	103.54213	8.8402418	0	49.596315	23.127142	10-1-0-
26	m	m	kPa	kPa	kPa	10 kPa
20	104.38528	9.132039	0	37.614468	17.539915	4015
	104.30320			kPa	kPa	10 kPa
Slice	m	m	kPa	IN U		
Slice 27	m		кра 0			
Slice 27 Slice 28		m 9.4697782 m		24.593615 kPa	11.468191 kPa	10 kPa

Slice	105.99414	9.8164592	0	14.041227	6.5475315	
29	m	m	kPa	kPa	kPa	
Slice	106.68243	10.166239	0	6.1328942	2.8598155	10 kPa
30	m	m	kPa	kPa	kPa	



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 19 Date: 10/12/2017 Time: 04:48:18 PM Tool Version: 9.0.2.15352 File Name: Torquay Section B-B Water at top of Dam.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:51:49 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (57.139, 16.28) m Left-Zone Right Coordinate: (80.05635, 16.40913) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (102, 10.48115) m Right-Zone Right Coordinate: (113.02256, 10.35) m Right-Zone Increment: 4 Radius Increments: 4

## **Slip Surface Limits**

Left Coordinate: (0, 9.46) m Right Coordinate: (113.706, 10.35) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	16.28 m
Coordinate 2	57.139 m	16.28 m

	Х	Y
Point 1	40 m	12.46 m

Deint	40.472	12.01	
Point	49.472	13.91	
2	m	m	
Point	57.139	16.28	
3	m	m	
Point	80.21 m	16.41	
4	00.21111	m	
Point	102.482	10.35	
5	m	m	
Point	111.706	10.35	
6	m	m	
Point	113.706	10.35	
7	m	m	
Point	113.706	-10 m	
8	m	-10 111	
Point	0	10	
9	0 m	-10 m	
Point	0 m	9.46	
10	0 m	m	
Point	20.403	9.46	
11	m	m	

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	2,576.7 m <sup>2</sup>

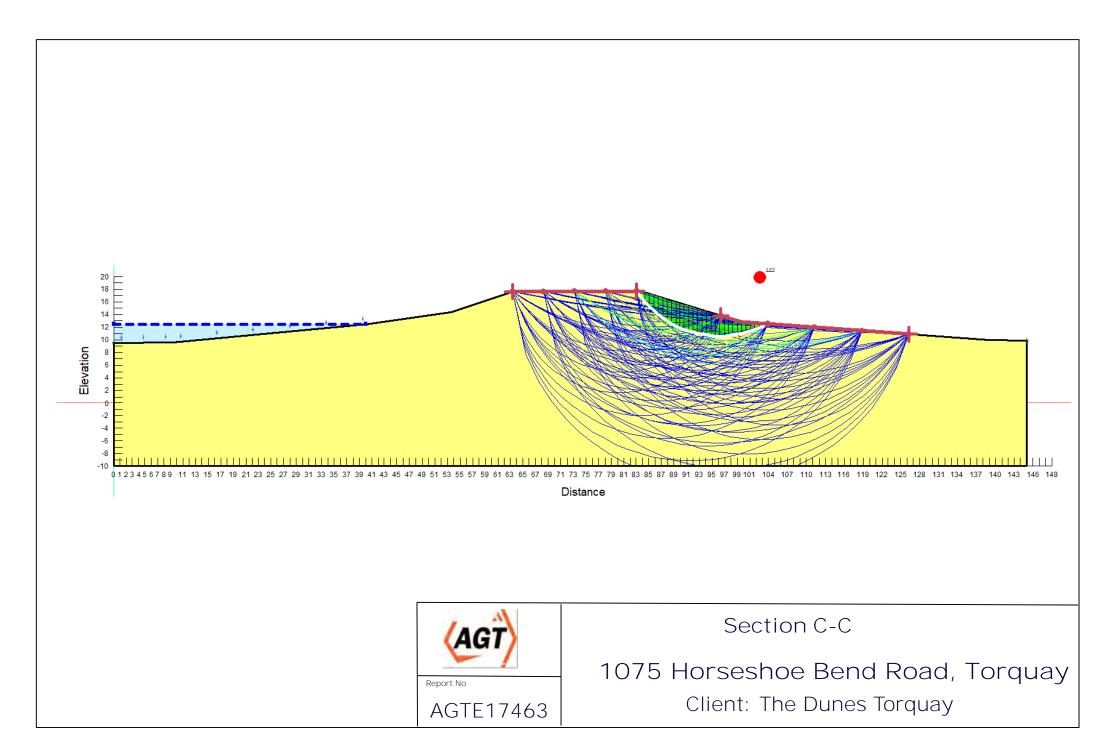
# **Current Slip Surface**

Slip Surface: 103 Factor of Safety: 2.977 Volume: 68.206704 m<sup>3</sup> Weight: 1,364.1341 kN Resisting Moment: 15,354.569 kN·m Activating Moment: 5,158.629 kN·m Resisting Force: 825.98086 kN Activating Force: 277.49676 kN Slip Rank: 1 of 125 slip surfaces Exit: (102, 10.481148) m Entry: (80.05635, 16.409134) m Radius: 17.018351 m Center: (94.331745, 25.67398) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	80.133175 m	16.292858 m	0 kPa	-2.193302 kPa	-1.0227535 kPa	10 kPa
Slice 2	80.573167 m	15.676776 m	0 kPa	6.5381288 kPa	3.0487795 kPa	10 kPa
Slice 3	81.2995 m	14.743954 m	0 kPa	18.808221 kPa	8.7704176 kPa	10 kPa

Slice	82.025833	13.930382		28.965811	13.506979	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	82.752167	13.212364	0	37.566595	17.517591	10 kPa
5	m	m	kPa	kPa	kPa	10 10 0
Slice 6	83.4785 m	12.574021 m	0 kPa	44.985108 kPa	20.9769 kPa	10 kPa
Slice	84.204833	12.004099	0	51.483387	24.007098	10 kPa
7	m	m	kPa	kPa	kPa	
Slice	84.931167	11.494293	0	57.247818	26.695096	10 kPa
8	m	m	kPa	kPa	kPa	
Slice 9	85.6575 m	11.038287 m	0 kPa	62.410421 kPa	29.102457 kPa	10 kPa
Slice	86.383833	10.631166	0	67.061786	31.271424	10 kPa
10	m	m	kPa	kPa	kPa	
Slice	87.110166	10.269039	0	71.259252	33.228735	10 kPa
11	m	m	kPa	kPa	kPa	
Slice 12	87.8365 m	9.9487879 m	0 kPa	75.032227 kPa	34.988102 kPa	10 kPa
Slice	88.562833	9.6678905	0	78.385819	36.551907	10 kPa
13	m	m	kPa	kPa	kPa	
Slice	89.289166	9.4243006	0	81.303475	37.912433	10 kPa
14	m	m	kPa	kPa	kPa	
Slice 15	90.0155 m	9.2163576 m	0 kPa	83.749192 kPa	39.05289 kPa	10 kPa
Slice	90.741833	9.0427213	0	85.669687	39.948431	10 kPa
16	m	m	kPa	kPa	kPa	
Slice	91.468166 m	8.9023238 m	0 kPa	86.996875 kPa	40.567309 kPa	10 kPa
Slice 18	92.1945 m	8.794334 m	0 kPa	87.650946 kPa	40.872307 kPa	10 kPa
Slice	92.920833	8.7181316	0	87.544233	40.822546	10 kPa
19	m	m	kPa	kPa	kPa	
Slice	93.647166	8.6732883	0	86.585993	40.375712	10 kPa
20	m	m	kPa	kPa	kPa	
Slice 21	94.3735 m	8.6595556 m	0 kPa	84.688063 kPa	39.490692 kPa	10 kPa
Slice	95.099833	8.6768581	0	81.771201	38.130537	10 kPa
22	m	m	kPa	kPa	kPa	
Slice	95.826166	8.7252909	0	77.771713	36.265545	10 kPa
23	m	m	kPa	kPa	kPa	
Slice 24	96.5525 m	8.8051227 m	0 kPa	72.647794 kPa	33.876223 kPa	10 kPa
Slice	97.278833	8.9168032	0	66.384859	30.955768	10 kPa
25	m	m	kPa	kPa	kPa	
Slice 26	98.005166 m	9.0609757 m	0 kPa	58.9991 kPa	27.511732 kPa	10 kPa
Slice	98.731499	9.2384973	0	50.538585	23.566529	10 kPa
27	m	m	kPa	kPa	kPa	
Slice	99.457833	9.450465	0	41.081415	19.156578	10 kPa
28	m	m	kPa	kPa	kPa	
						10 kPa

Slice	100.18417	9.698253	0	30.730825	14.330019	
29	m	m	kPa	kPa	kPa	
Slice	100.9105	9.9835629	0	19.607494	9.1431246	10 kPa
30	m	m	kPa	kPa	kPa	IU KPd
Slice	101.63683	10.30849	0	7.8397142	3.6557188	10 kPa
31	m	m	kPa	kPa	kPa	то кра



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 19 Date: 10/12/2017 Time: 04:50:57 PM Tool Version: 9.0.2.15352 File Name: Torquay Section C-C.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:35:09 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (63.377, 17.66) m Left-Zone Right Coordinate: (83.03952, 17.73771) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (96.4588, 13.84343) m Right-Zone Right Coordinate: (126.27574, 10.90975) m Right-Zone Increment: 4 Radius Increments: 4

## **Slip Surface Limits**

Left Coordinate: (0, 9.45) m Right Coordinate: (145, 9.93) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	12.49 m
Coordinate 2	40 m	12.49 m

	Х	Y
Point 1	40 m	12.49 m

Point	53.462	14.47
2	m	m
Point	63.377	17.66
3	m	m
Point	83.62 m	17.74
4	05.02 111	m
Point	99.765	12.84
5	m	m
Point	138.908	9.99
6	m	m
Point	145 m	9.93
7	145 111	m
Point	145 m	-10 m
8	1.0	10
Point	0 m	-10 m
9	UIII	10111
Point	0 m	9.45
10	UIII	m
Point	9.49 m	9.603
11	5.45 111	m

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	3,330.8 m <sup>2</sup>

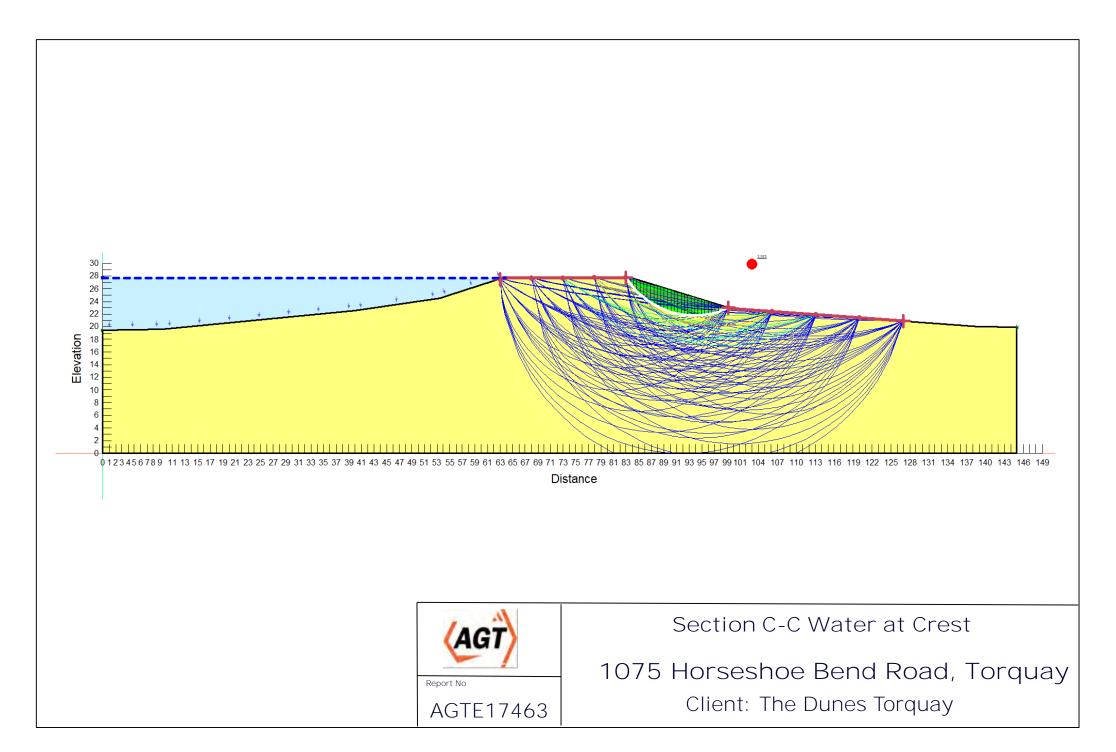
# **Current Slip Surface**

Slip Surface: 108 Factor of Safety: 2.975 Volume: 55.338124 m<sup>3</sup> Weight: 1,106.7625 kN Resisting Moment: 12,098.604 kN·m Activating Moment: 4,066.8428 kN·m Resisting Force: 698.47712 kN Activating Force: 234.78224 kN Slip Rank: 1 of 125 slip surfaces Exit: (103.80819, 12.545616) m Entry: (83.03952, 17.737706) m Radius: 15.798625 m Center: (96.242062, 26.414656) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	83.32976 m	17.325388 m	0 kPa	2.8534822 kPa	1.3306006 kPa	10 kPa
Slice 2	83.970978 m	16.479568 m	0 kPa	15.301696 kPa	7.1352981 kPa	10 kPa
Slice 3	84.672935 m	15.668219 m	0 kPa	25.278137 kPa	11.787389 kPa	10 kPa

Slice	85.374891	14.957468	0	33.577787	15.657579	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	86.076848	14.329348	0	40.615343	18.939245	
5	m	m	kPa	kPa	kPa	10 kPa
Slice	86.778804	13.771431	0		21.764644	1015
6	m	m	kPa	46.67443 kPa	kPa	10 kPa
Slice	87.480761	13.274708	0	51.953241	24.226194	
7	m	m	kPa	kPa	kPa	10 kPa
Slice	88.182717	12.832426	0	56.590078	26.388387	
8	m	m	kPa	kPa	kPa	10 kPa
Slice	88.884674	12.439389	0		28.294877	4010
9	m	m	kPa	60.67856 kPa	kPa	10 kPa
Slice	89.58663	12.091527	0	64.277096	29.972902	
10	m	m	kPa	kPa	kPa	10 kPa
Slice	90.288587	11.785605	0		31.436145	
11	m	m	kPa	67.41503 kPa	kPa	10 kPa
Slice	90.990543	11.519031	0	70.096825	32.686686	
12	m	m	kPa	kPa	kPa	10 kPa
Slice		11.289719	0	72.305143	33.716442	
13	91.6925 m	m	kPa	kPa	kPa	10 kPa
Slice	92.394457	11.095989	0	74.003429	34.508366	
311CE 14	m	m	kPa	kPa	kPa	10 kPa
Slice	93.096413	10.936504	0		Ki û	
15	m	m	kPa	75.13844 kPa	35.03763 kPa	10 kPa
			+		25 272052	
Slice 16	93.79837	10.81021	0 kPa	75.64309 kPa	35.272952 kPa	10 kPa
	m	m		75 420805		
Slice 17	94.500326 m	10.716305 m	0 kPa	75.439895 kPa	35.178201 kPa	10 kPa
			0			
Slice 18	95.202283 m	10.654208 m	kPa	74.445226 kPa	34.714379 kPa	10 kPa
	95.904239		0			
Slice 19	95.904239 m	10.623544 m	kPa	72.574429 kPa	33.842012 kPa	10 kPa
					ΝΓα	
Slice 20	96.606196	10.62413	0 kPa	69.747771 kPa	32.52392 kPa	10 kPa
	m	m				
Slice	97.308152	10.655967	0	65.896923	30.72824 kPa	10 kPa
21	m	m	kPa	kPa		
Slice	98.010109	10.719248	0	60.97153 kPa	28.431491	10 kPa
22	m	m	kPa		kPa	
Slice	98.712065	10.814355	0	54.945216	25.621375	10 kPa
23	m	m	kPa	kPa	kPa	
Slice	99.414022	10.941877	0	47.82024 kPa	22.298944	10 kPa
24	m	m	kPa		kPa	-
Slice	100.10193	11.098742	0	41.521945	19.362001	10 kPa
25	m	m	kPa	kPa	kPa	
Slice	100.7758	11.284617	0	36.153252	16.858538	10 kPa
26	m	m	kPa	kPa	kPa	
Slice	101.44966	11.503248	0	29.892471	13.939088	10 kPa
27	m	m	kPa	kPa	kPa	TO KEQ
Slice	102.12353	11.756104	0	22.798498	10.631114	10 kPa
	-	m	kPa	kPa	kPa	TO KPd
28	m		NI U			

Slice 29	102.79739 m	12.044998 m	0 kPa		6.9685858 kPa	
Slice 30	103.47126 m	12.37216 m	0 kPa	6.4096737 kPa	2.98888 kPa	10 kPa



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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 21 Date: 10/12/2017 Time: 04:49:22 PM Tool Version: 9.0.2.15352 File Name: Torquay Section C-C Water at top of Dam.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:59:36 PM

## **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

## **Materials**

### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (63, 27.53871) m Left-Zone Right Coordinate: (83, 27.73755) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (99.23782, 23) m Right-Zone Right Coordinate: (127, 20.85702) m Right-Zone Increment: 4 Radius Increments: 4

## **Slip Surface Limits**

Left Coordinate: (0, 19.45) m Right Coordinate: (145, 19.93) m

## **Piezometric Lines**

### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	27.66 m
Coordinate 2	63.77 m	27.66 m

	Х	Y
Point 1	40 m	22.49 m

Point 2	53.462 m	24.47 m
Point 3	63.377 m	27.66 m
Point 4	83.62 m	27.74 m
Point 5	99.765 m	22.84 m
Point 6	138.908 m	19.99 m
Point 7	145 m	19.93 m
Point 8	145 m	0 m
Point 9	0 m	0 m
Point 10	0 m	19.45 m
Point 11	9.49 m	19.603 m

# Regions

	Material	Points	Area
Region 1	Sandy Clay	1,11,10,9,8,7,6,5,4,3,2	3,330.8 m <sup>2</sup>

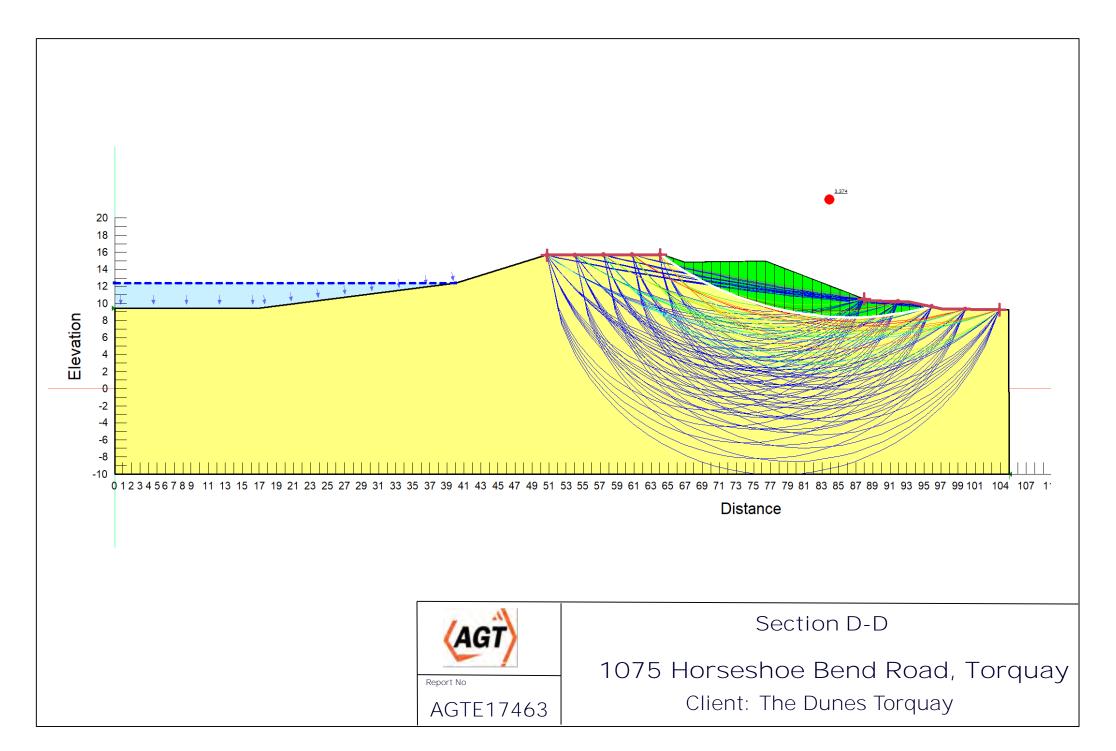
# **Current Slip Surface**

Slip Surface: 103 Factor of Safety: 2.923 Volume: 38.184594 m<sup>3</sup> Weight: 763.69189 kN Resisting Moment: 7,044.7854 kN·m Activating Moment: 2,409.3894 kN·m Resisting Force: 498.25278 kN Activating Force: 170.45591 kN Slip Rank: 1 of 125 slip surfaces Exit: (99.23782, 22.999999) m Entry: (83, 27.73755) m Radius: 12.863183 m Center: (93.833455, 34.672802) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	83.31 m	27.295355 m	0 kPa	3.2321308 kPa	1.5071673 kPa	10 kPa
Slice 2	83.889273 m	26.524538 m	0 kPa	14.812981 kPa	6.9074066 kPa	10 kPa
Slice 3	84.427818 m	25.906989 m	0 kPa	22.32466 kPa	10.41016 kPa	10 kPa

Slice	84.966364	25.361631	0	28.640993	13.355514	10 kPa
4	m	m	kPa	kPa	kPa	
Slice	85.504909	24.876278	0	34.061305	15.883047	10 00
5	m	m	kPa	kPa	kPa	10 kPa
Slice	86.043455	24.442317	0	38.792778	40,00027.60-	10.00
6	m	m	kPa	kPa	18.08937 kPa	10 kPa
Slice	06 502	24.053406	0	42.981612	20.042655	1010
7	86.582 m	m	kPa	kPa	kPa	10 kPa
Slice	87.120546	23.704727	0	46.730757	24 70004   D	4010
8	m	m	kPa	kPa	21.79091 kPa	10 kPa
Slice	87.659091	23.392533	0	50.110588	23.366951	1010
9	m	m	kPa	kPa	kPa	10 kPa
Slice	88.197637	23.113854	0	53.165554	24.791505	
10	m	m	kPa	kPa	kPa	10 kPa
Slice	88.736182	22.866309	0	55.918472	26.075212	
11	m	m	kPa	kPa	kPa	10 kPa
Slice	89.274728	22.647971	0	58.373388	27.219958	
12	m	m	kPa	kPa	kPa	10 kPa
Slice	89.813273	22.457268	0			
13	m	22.457268 m	kPa	60.51762 kPa	28.21983 kPa	10 kPa
Slice	90.351819	22.292921	0	62.323432	29.061894	
311Ce 14	90.551819 m	m	kPa	kPa	kPa	10 kPa
				кга	кга	
Slice 15	90.890364	22.153889	0	63.74965 kPa	29.72695 kPa	10 kPa
	m	m	kPa		20.400404	
Slice	91.42891	22.039334	0	64.74353 kPa	30.190404	10 kPa
16	m	m	kPa		kPa	
Slice	91.967455	21.948594	0	65.2431 kPa	30.423357	10 kPa
17	m	m	kPa		kPa	
Slice	92.506001	21.881162	0	65.180162	30.394009	10 kPa
18	m	m	kPa	kPa	kPa	
Slice	93.044546	21.836668	0	64.48405 kPa	30.069406	10 kPa
19	m	m	kPa		kPa	
Slice	93.583092	21.814876	0	63.086143	29.417551	10 kPa
20	m	m	kPa	kPa	kPa	10 11 0
Slice	94.121637	21.815668	0	60.924975	28.409782	10 kPa
21	m	m	kPa	kPa	kPa	IUKFd
Slice	94.660183	21.83905	0	57.951624	27.023286	10 kPa
22	m	m	kPa	kPa	kPa	IU KPa
Slice	95.198728	21.885145	0	54.134895	25.243516	10.00
23	m	m	kPa	kPa	kPa	10 kPa
Slice	95.737274	24.07.5	0	49.465706	23.066237	1015
24	m	21.9542 m	kPa	kPa	kPa	10 kPa
Slice	96.275819	22.046594	0	43.960011		
25	m	m	kPa	kPa	20.49889 kPa	10 kPa
Slice	96.814365	22.162844	0	37.659695	17.561004	
26	m	m	kPa	kPa	kPa	10 kPa
Slice	97.35291	22.303625	0	30.631039	14.283488	
27	97.35291 m	m	kPa	kPa	kPa	10 kPa
Slice	97.891456	22.469786		22.960669	10.706736	10 kPa
28	m	m	kPa	kPa 14.74926 kPa	kPa	10 kPa

Slice 29	98.430001 m	22.662385 m	0 kPa		6.8776931 kPa	
Slice	98.968547	22.882719	0	6.1035763	2.8461444	10 kPa
30	m	m	kPa	kPa	kPa	



# **Slope Stability**

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### **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 19 Date: 10/12/2017 Time: 04:49:39 PM Tool Version: 9.0.2.15352 File Name: Torquay Section D-D.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:39:01 PM

### **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

**Slope Stability** Kind: SLOPE/W Method: Morgenstern-Price Settings Side Function Interslice force function option: Half-Sine **PWP Conditions from: Piezometric Line** Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 9.807 kN/m<sup>3</sup> Slip Surface Direction of movement: Left to Right Use Passive Mode: No Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1 Optimize Critical Slip Surface Location: No Tension Crack Option: (none) Distribution F of S Calculation Option: Constant Advanced **Geometry Settings** Minimum Slip Surface Depth: 0.1 m Number of Slices: 30 Factor of Safety Convergence Settings Maximum Number of Iterations: 100

### **Materials**

#### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (50.75385, 15.66334) m Left-Zone Right Coordinate: (64.04935, 15.72897) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (88, 10.53052) m Right-Zone Right Coordinate: (103.86049, 9.29522) m Right-Zone Increment: 4 Radius Increments: 4

# **Slip Surface Limits**

Left Coordinate: (0, 9.45) m Right Coordinate: (105, -10) m

### **Piezometric Lines**

#### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	12.38 m
Coordinate 2	40 m	12.38 m

#### **Points**

	Х	Y
Point 1	40 m	12.38 m

Point 2	50.684 m	15.663 m
Point 3	64.259 m	15.73 m
Point 4	66.89 m	14.82 m
Point 5	76.408 m	14.94 m
Point 6	88.422 m	10.37 m
Point 7	93.324 m	10.14 m
Point 8	97.068 m	9.39 m
Point 9	104.951 m	9.28 m
Point 10	0 m	9.45 m
Point 11	16.936 m	9.45 m
Point 12	105 m	-10 m
Point 13	0 m	-10 m

# Regions

	Material	Points	Area
Region 1	Sandy Clay	10,13,12,9,8,7,6,5,4,3,2,1,11	2,318.9 m²

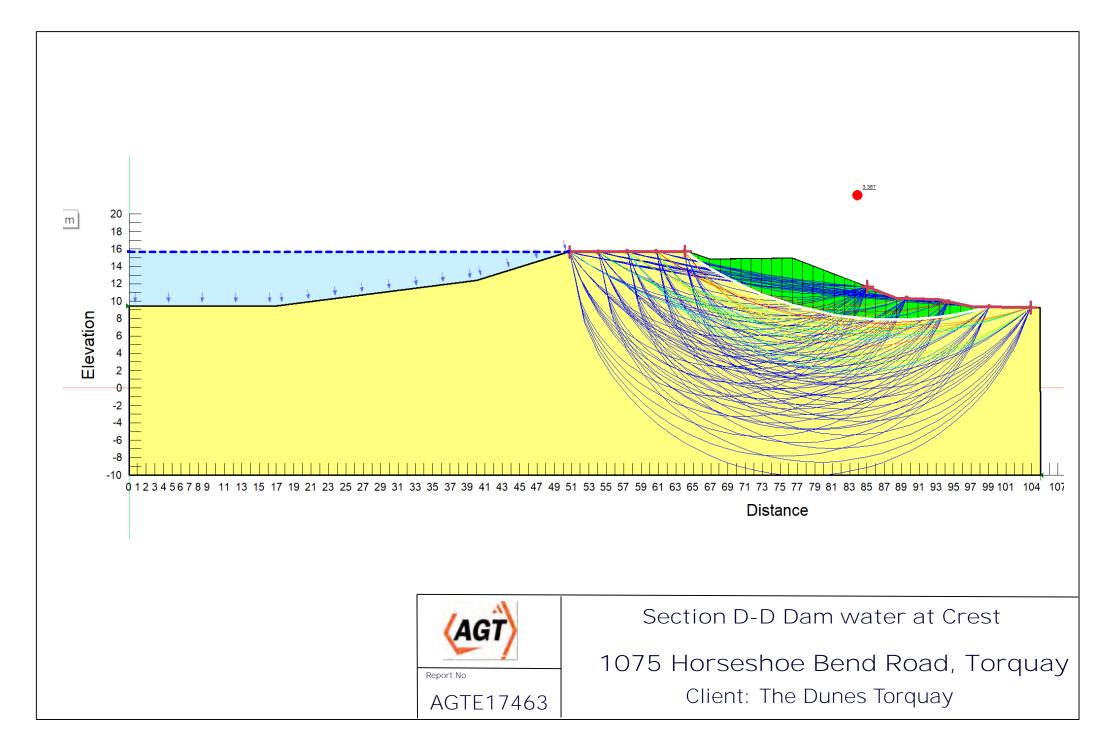
# **Current Slip Surface**

Slip Surface: 112 Factor of Safety: 3.374 Volume: 89.518973 m<sup>3</sup> Weight: 1,790.3795 kN Resisting Moment: 43,862.64 kN·m Activating Moment: 13,000.775 kN·m Resisting Force: 1,123.4653 kN Activating Force: 332.99582 kN Slip Rank: 1 of 125 slip surfaces Exit: (95.899161, 9.6241425) m Entry: (64.04935, 15.728965) m Radius: 37.511784 m Center: (86.341991, 45.898023) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice	64.154175	15.652068	0	-0.55680022	-0.25964021	10 kPa
1	m	m	kPa	kPa	kPa	TOKIG

Slice	64.91675	15.117336	0	5.1589695 kPa	2.405667 kPa	10 kPa
2	m	m	kPa			
Slice 3	66.23225 m	14.241665 m	0 kPa	12.935311 kPa	6.0318347 kPa	10 kPa
Slice 4	67.418778 m	13.514836 m	0 kPa	22.168887 kPa	10.337522 kPa	10 kPa
Slice	68.476333	12.919386	0 kPa	33.228278 kPa	15.494601 kPa	10 kPa
Slice	m 69.533889	m 12.367862	0	43.533647 kPa	20.300073	10 kPa
6 Slice	m 70.591444	m 11.858124	kPa 0	53.179883 kPa	kPa 24.798187	10 kPa
7 Slice	m	m 11.38832	kPa 0		kPa 29.025276	
8 Slice	71.649 m	m 10.956835	kPa	62.244906 kPa	kPa	10 kPa
9	72.706556 m	m	0 kPa	70.790535 kPa	33.010168 kPa	10 kPa
Slice 10	73.764111 m	10.562265 m	0 kPa	78.863188 kPa	36.774509 kPa	10 kPa
Slice 11	74.821667 m	10.203384 m	0 kPa	86.494471 kPa	40.333034 kPa	10 kPa
Slice 12	75.879222 m	9.879123 m	0 kPa	93.701716 kPa	43.693828 kPa	10 kPa
Slice 13	76.954091 m	9.5843469 m	0 kPa	96.531632 kPa	45.013439 kPa	10 kPa
Slice	78.046273 m	9.3193216 m	0 kPa	94.851283 kPa	44.22988 kPa	10 kPa
Slice	79.138455 m	9.0886042 m	0 kPa	92.529239 kPa	43.147093 kPa	10 kPa
Slice 16	80.230636 m	8.8915521 m	0 kPa	89.521731 kPa	41.744669 kPa	10 kPa
Slice	81.322818 m	8.7276297 m	0 kPa	85.783732 kPa	40.001611 kPa	10 kPa
Slice	82.415 m	8.5963996 m	0 kPa	81.271683 kPa	37.897608 kPa	10 kPa
Slice	83.507182	8.4975174	0	75.946351 kPa	35.414365	10 kPa
19 Slice	m 84.599364	m 8.4307269	kPa 0	69.775674 kPa	kPa 32.536931	10 kPa
20 Slice	m 85.691545	m 8.3958563	kPa 0	62.737437 kPa	kPa 29.254947	10 kPa
21 Slice	m 86.783727	m 8.3928166	kPa 0	54.821556 kPa	kPa 25.563711	10 kPa
22 Slice	m 87.875909	m 8.4216001	kPa 0		kPa 21.464962	
23 Slice	m	m 8.477621	kPa 0	46.03176 kPa	kPa 18.789987	10 kPa
24	88.9122 m	m	kPa	40.295257 kPa	kPa	10 kPa
Slice 25	89.8926 m	8.5579025 m	0 kPa	37.751439 kPa	17.603785 kPa	10 kPa
Slice 26	90.873 m	8.6641675 m	0 kPa	34.573586 kPa	16.121928 kPa	10 kPa
	91.8534 m			30.770662 kPa		10 kPa

Slice 27		8.7966394 m	0 kPa		14.348595 kPa	
Slice 28	92.8338 m	8.9556003 m	0 kPa	26.357632 kPa	12.290766 kPa	10 kPa
Slice	93.96779	9.1754313	0	18.418636	8.5887509	10 kPa
29	m	m	kPa	kPa	kPa	
Slice	95.25537	9.4666315	0	6.8157015	3.1782138	10 kPa
30	m	m	kPa	kPa	kPa	



# **Slope Stability**

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## **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 22 Date: 10/12/2017 Time: 04:49:04 PM Tool Version: 9.0.2.15352 File Name: Torquay Section D-D Water at top of Dam.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 10/12/2017 Last Solved Time: 05:55:39 PM

### **Project Settings**

Unit System: International System of Units (SI)

# **Analysis Settings**

**Slope Stability** Kind: SLOPE/W Method: Morgenstern-Price Settings Side Function Interslice force function option: Half-Sine **PWP Conditions from: Piezometric Line** Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 9.807 kN/m<sup>3</sup> Slip Surface Direction of movement: Left to Right Use Passive Mode: No Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1 Optimize Critical Slip Surface Location: No Tension Crack Option: (none) Distribution F of S Calculation Option: Constant Advanced **Geometry Settings** Minimum Slip Surface Depth: 0.1 m Number of Slices: 30 Factor of Safety Convergence Settings Maximum Number of Iterations: 100

### **Materials**

#### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (50.75385, 15.66334) m Left-Zone Right Coordinate: (64.04935, 15.72897) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (85.03854, 11.65703) m Right-Zone Right Coordinate: (103.86049, 9.29522) m Right-Zone Increment: 4 Radius Increments: 4

# **Slip Surface Limits**

Left Coordinate: (0, 9.45) m Right Coordinate: (105, -10) m

### **Piezometric Lines**

#### **Piezometric Line 1**

#### Coordinates

	Х	Y
Coordinate 1	0 m	15.663 m
Coordinate 2	50.684 m	15.663 m

#### **Points**

	Х	Y
Point 1	40 m	12.38 m

Point 2	50.684 m	15.663 m
Point 3	64.259 m	15.73 m
Point 4	66.89 m	14.82 m
Point 5	76.408 m	14.94 m
Point 6	88.422 m	10.37 m
Point 7	93.324 m	10.14 m
Point 8	97.068 m	9.39 m
Point 9	104.951 m	9.28 m
Point 10	0 m	9.45 m
Point 11	16.936 m	9.45 m
Point 12	105 m	-10 m
Point 13	0 m	-10 m

# Regions

	Material	Points	Area
Region 1	Sandy Clay	10,13,12,9,8,7,6,5,4,3,2,1,11	2,318.9 m²

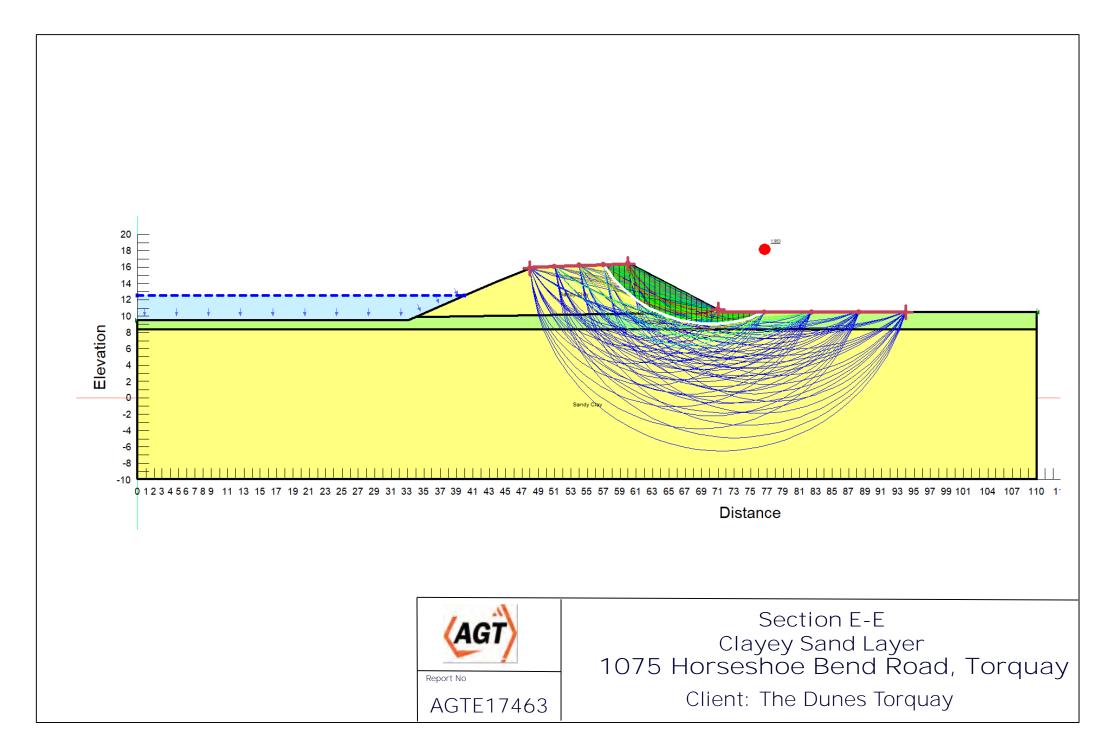
# **Current Slip Surface**

Slip Surface: 117 Factor of Safety: 3.367 Volume: 101.23961 m<sup>3</sup> Weight: 2,024.7923 kN Resisting Moment: 53,586.278 kN·m Activating Moment: 15,915.611 kN·m Resisting Force: 1,261.4287 kN Activating Force: 374.66059 kN Slip Rank: 1 of 125 slip surfaces Exit: (99.07623, 9.361977) m Entry: (64.04935, 15.728965) m Radius: 40.820542 m Center: (88.132616, 48.688227) m

	x	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	64.154175 m	15.652879 m	0 kPa	-0.55641138 kPa	-0.25945889 kPa	10 kPa

Slice	64.91675	15.121866	0	5.086465 kPa	2.3718576	10 kPa
2	m	m	kPa		kPa	
Slice 3	66.23225 m	14.248671 m	0 kPa	12.817715 kPa	5.9769986 kPa	10 kPa
Slice 4	67.484875 m	13.481525 m	0 kPa	22.804825 kPa	10.634065 kPa	10 kPa
Slice	68.674625	12.810027	0	35.283195 kPa	16.452824	10 kPa
5	m	m	kPa		kPa	
Slice 6	69.864375 m	12.189659 m	0 kPa	46.87766 kPa	21.859412 kPa	10 kPa
Slice 7	71.054125 m	11.617851 m	0 kPa	57.700326 kPa	26.906104 kPa	10 kPa
Slice 8	72.243875 m	11.092383 m	0 kPa	67.842983 kPa	31.635703 kPa	10 kPa
Slice	73.433625	10.611335	0	77.378175 kPa	36.082036	10 kPa
9	m	m	kPa		kPa	
Slice 10	74.623375 m	10.17304 m	0 kPa	86.360051 kPa	40.270353 kPa	10 kPa
Slice 11	75.813125 m	9.7760512 m	0 kPa	94.825088 kPa	44.217665 kPa	10 kPa
Slice 12	77.0087 m	9.4175595 m	0 kPa	98.390807 kPa	45.880387 kPa	10 kPa
Slice 13	78.2101 m	9.0968542 m	0 kPa	96.941004 kPa	45.204333 kPa	10 kPa
Slice	79.4115 m	8.8149194 m	0 kPa	94.806201 kPa	44.208857 kPa	10 kPa
Slice	80.6129 m	8.5709367 m	0 kPa	91.944746 kPa	42.874539 kPa	10 kPa
Slice	81.8143 m	8.3642167 m	0 kPa	88.311392 kPa	41.180278 kPa	10 kPa
Slice	83.0157 m	8.194188 m	0 kPa	83.860049 kPa	39.104583 kPa	10 kPa
Slice	84.2171 m	8.0603897	0 kPa	78.546744 kPa	36.626948 kPa	10 kPa
Slice	85.4185 m	m 7.9624642	0 kPa	72.33266 kPa	33.729273 kPa	10 kPa
Slice	86.6199 m	m 7.900153	0 kPa	65.187148 kPa	30.397266 kPa	10 kPa
Slice	87.8213 m	m 7.8732929	0 kPa	57.090491 kPa	26.621733 kPa	10 kPa
Slice	89.03475	m 7.8822577	0	52.127719 kPa	24.307554	10 kPa
22	m	m	kPa		kPa	
Slice 23	90.26025 m	7.927789 m	0 kPa	50.34889 kPa	23.478073 kPa	10 kPa
Slice 24	91.48575 m	8.0102833 m	0 kPa	47.651312 kPa	22.220172 kPa	10 kPa
Slice 25	92.71125 m	8.1299666 m	0 kPa	44.029771 kPa	20.53142 kPa	10 kPa
		8.2889636	0	37.447056 kPa	17.461849	10 kPa
Slice 26	93.948 m	m	kPa		kPa	

Slice 27		8.4884281 m	0 kPa		13.015455 kPa	
Slice 28	96.444 m	8.7278554 m	0 kPa	17.512276 kPa	8.1661084 kPa	10 kPa
Slice 29	97.570057 m	8.9769563 m	0 kPa	9.4212941 kPa	4.3932216 kPa	10 kPa
Slice 30	98.574172 m	9.229124 m	0 kPa	3.795612 kPa	1.7699229 kPa	10 kPa



# **Clayey Sand**

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### **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 25 Date: 10/12/2017 Time: 07:52:37 PM Tool Version: 9.0.2.15352 File Name: Torquay Section E-E.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 11/12/2017 Last Solved Time: 07:33:44 AM

### **Project Settings**

Unit System: International System of Units (SI)

## **Analysis Settings**

**Clayey Sand** Kind: SLOPE/W Method: Morgenstern-Price Settings Side Function Interslice force function option: Half-Sine **PWP Conditions from: Piezometric Line** Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 9.807 kN/m<sup>3</sup> Slip Surface Direction of movement: Left to Right Use Passive Mode: No Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1 Optimize Critical Slip Surface Location: No Tension Crack Option: (none) Distribution F of S Calculation Option: Constant Advanced **Geometry Settings** Minimum Slip Surface Depth: 0.1 m Number of Slices: 30 Factor of Safety Convergence Settings Maximum Number of Iterations: 100

### **Materials**

#### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

#### **Clayey Sand**

Model: Mohr-Coulomb Unit Weight: 18 kN/m<sup>3</sup> Cohesion': 2 kPa Phi': 30 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (48, 15.83419) m Left-Zone Right Coordinate: (60, 16.38362) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (71, 10.79286) m Right-Zone Right Coordinate: (94, 10.51) m Right-Zone Increment: 4 Radius Increments: 4

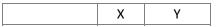
### **Slip Surface Limits**

Left Coordinate: (0, 9.47) m Right Coordinate: (110, 10.51) m

### **Piezometric Lines**

#### **Piezometric Line 1**

#### **Coordinates**



Coordinate	0	12.49
1	m	m
Coordinate	40	12.49
2	m	m

### **Points**

	Х	Y
Point 1	40 m	12.47 m
Point 2	43.744 m	14.09 m
Point 3	48.307 m	15.96 m
Point 4	60.176 m	16.39 m
Point 5	71.547 m	10.51 m
Point 6	110 m	10.51 m
Point 7	110 m	-10 m
Point 8	0 m	-10 m
Point 9	0 m	9.47 m
Point 10	33.0667 m	9.47 m
Point 11	33.96945 m	9.86061 m
Point 12	0 m	8.39 m
Point 13	110 m	8.39 m

# Regions

	Material	Points	Area
Region 1	Sandy Clay	1,11,5,4,3,2	147.79 m²
Region 2	Clayey Sand	10,9,12,13,6,5,11	185.85 m²
Region 3	Sandy Clay	8,7,13,12	2,022.9 m <sup>2</sup>

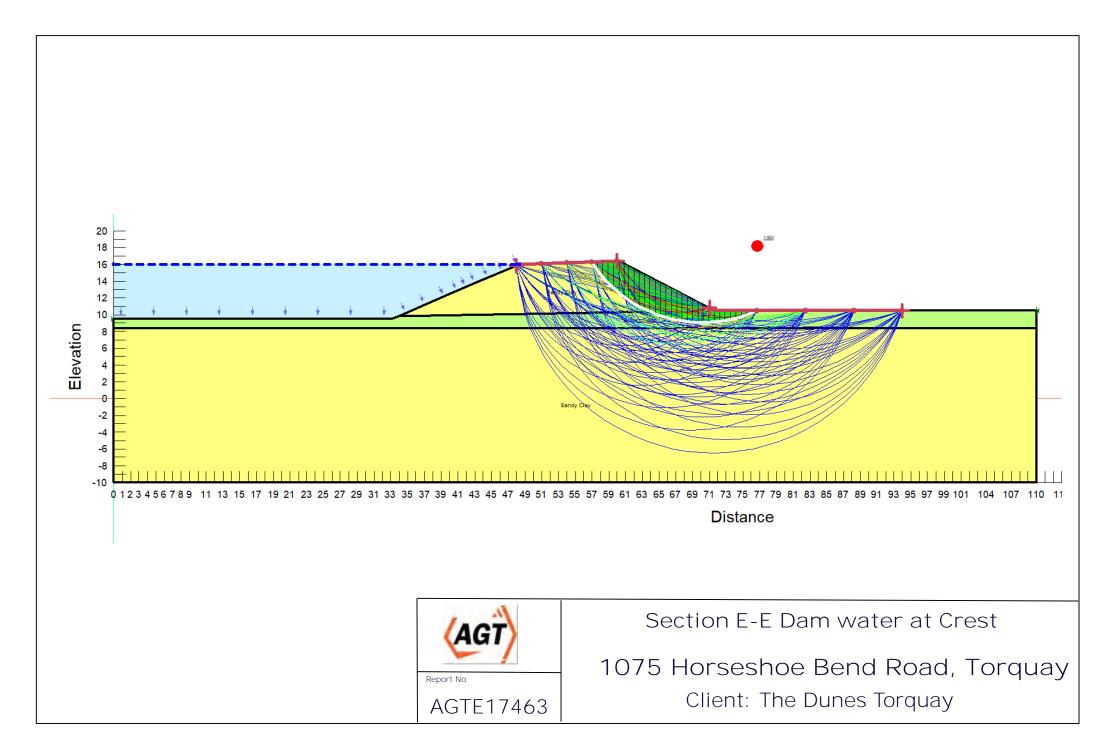
# **Current Slip Surface**

Slip Surface: 83 Factor of Safety: 1.953 Volume: 49.187049 m<sup>3</sup> Weight: 959.5182 kN Resisting Moment: 9,726.6361 kN·m Activating Moment: 4,980.2654 kN·m Resisting Force: 555.45852 kN Activating Force: 284.50158 kN Slip Rank: 1 of 125 slip surfaces Exit: (76.698394, 10.51) m Entry: (56.99386, 16.274715) m Radius: 15.621786 m Center: (70.152579, 24.694234) m

	х	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	57.312074 m	15.81456 m	0 kPa	1.5931883 kPa	0.74291589 kPa	10 kPa

Slice	57.948502	14.95563	0	15.432752	7.1964103	10 kDa
2	m	m	kPa	kPa	kPa	10 kPa
Slice 3	58.58493 m	14.205895 m	0 kPa	27.503465 kPa	12.825076 kPa	10 kPa
Slice	59.221358	13.542999	0	38.308393	17.863497	10 kPa
4	m	m	kPa	kPa	kPa	
Slice 5	59.857786 m	12.952073 m	0 kPa	48.202651 kPa	22.477265 kPa	10 kPa
Slice	60.486419	12.428454	0 kPa	54.688407	25.501623	10 kPa
6	m	m		kPa	kPa	
Slice 7	61.107258 m	11.963273 m	0 kPa	57.863793 kPa	26.98233 kPa	10 kPa
Slice	61.728096	11.543858	0	60.590893	28.253997	10 10
8	m	m	kPa	kPa	kPa	10 kPa
Slice	62.348935	11.165934	0	62.923804	29.341852	10 kPa
9	m	m	kPa	kPa	kPa	
Slice 10	62.969774 m	10.826094 m	0 kPa	64.890644 kPa	30.259004 kPa	10 kPa
Slice	63.590612	10.521592	0	66.497586	31.008334	10 kPa
11	m	m	kPa	kPa	kPa	
Slice 12	64.219614 m	10.247037 m	0 kPa	67.52588 kPa	38.986085 kPa	2 kPa
Slice	64.856778	10.001379	0	67.889748	39.196164	2 1/00
13	m	m	kPa	kPa	kPa	2 kPa
Slice	65.493942	9.7869913	0	67.817683	39.154557	2 kPa
14	m	m	kPa	kPa	kPa	ZKFd
Slice	66.131106	9.6025394	0	67.241526	38.821913	2 kPa
15	m	m	kPa	kPa	kPa	2 11 0
Slice	66.76827	9.4469342	0	66.082619	38.152818	2 kPa
16	m	m	kPa	kPa	kPa	
Slice	67.405434	9.3192981	0	64.255295	37.097812	2 kPa
17	m	m	kPa	kPa	kPa	
Slice	68.042598	9.2189378	0	61.671472	35.606041	2 kPa
18	m	m	kPa	kPa	kPa	
Slice	68.679762	9.1453241	0	58.246405	33.628578	2 kPa
19	m	m	kPa	kPa	kPa	
Slice	69.316926	9.0980777	0	53.905501	31.122355	2 kPa
20	m	m	kPa	kPa	kPa	
Slice	69.95409	9.0769588	0	48.591812	28.054496	2 kPa
21	m	m	kPa	kPa	kPa	
Slice	70.591254	9.0818612	0	42.273574	24.406659	2 kPa
22	m	m	kPa	kPa	kPa	
Slice	71.228418	9.1128096	0	34.950865	20.178891	2 kPa
23	m	m	kPa	kPa	kPa	
Slice 24	71.868962 m	9.1704041 m	0 kPa	30.424452 kPa	17.565566 kPa	2 kPa
Slice	72.512886	9.255223	0	20 02742 50-	16.649298	2 40-
25	m	m	kPa	28.83743 kPa	kPa	2 kPa
Slice	73.156811	9.3675532	0	26.429987	15 25020 -	2 40-
26	m	m	kPa	kPa	15.25936 kPa	2 kPa
			1	1	1	1

Slice	73.800735	9.5080064	0	23.221425	13.406896	
27	m	m	kPa	kPa	kPa	
Slice	74.444659	9.6773731	0	19.256254	11.117603	2 kPa
28	m	m	kPa	kPa	kPa	
Slice	75.088584	9.8766468	0	14.600272	8.4294708	2 kPa
29	m	m	kPa	kPa	kPa	
Slice	75.732508	10.107056	0	9.3339166	5.3889393	2 kPa
30	m	m	kPa	kPa	kPa	
Slice	76.376432	10.370107	0	3.5436844	2.0459471	2 kPa
31	m	m	kPa	kPa	kPa	



# **Clayey Sand**

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### **File Information**

File Version: 9.00 Title: Torquay Created By: Matt Noonan Last Edited By: Matt Noonan Revision Number: 27 Date: 10/12/2017 Time: 08:11:13 PM Tool Version: 9.0.2.15352 File Name: Torquay Section E-E Water at top of Dam.gsz Directory: C:\Users\mattn\Documents\AGT\~ Projects\AGTE17463 The Dunes Torquay - 1075 Horseshoe Bend Road, Torquay\Slope W\ Last Solved Date: 11/12/2017 Last Solved Time: 07:35:05 AM

### **Project Settings**

Unit System: International System of Units (SI)

## **Analysis Settings**

**Clayey Sand** Kind: SLOPE/W Method: Morgenstern-Price Settings Side Function Interslice force function option: Half-Sine **PWP Conditions from: Piezometric Line** Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 9.807 kN/m<sup>3</sup> Slip Surface Direction of movement: Left to Right Use Passive Mode: No Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1 Optimize Critical Slip Surface Location: No Tension Crack Option: (none) Distribution F of S Calculation Option: Constant Advanced **Geometry Settings** Minimum Slip Surface Depth: 0.1 m Number of Slices: 30 Factor of Safety Convergence Settings Maximum Number of Iterations: 100

### **Materials**

#### **Sandy Clay**

Model: Mohr-Coulomb Unit Weight: 20 kN/m<sup>3</sup> Cohesion': 10 kPa Phi': 25 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

#### **Clayey Sand**

Model: Mohr-Coulomb Unit Weight: 18 kN/m<sup>3</sup> Cohesion': 2 kPa Phi': 30 ° Phi-B: 0 ° Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range Left-Zone Left Coordinate: (48, 15.83419) m Left-Zone Right Coordinate: (60, 16.38362) m Left-Zone Increment: 4 Right Type: Range Right-Zone Left Coordinate: (71, 10.79286) m Right-Zone Right Coordinate: (94, 10.51) m Right-Zone Increment: 4 Radius Increments: 4

### **Slip Surface Limits**

Left Coordinate: (0, 9.47) m Right Coordinate: (110, 10.51) m

### **Piezometric Lines**

#### **Piezometric Line 1**

#### Coordinates

|--|

Coordinate	0 m	15.96	
1		m	
Coordinate	48.307	15.96	
2	m	m	

### **Points**

	Х	Y	
Point 1	40 m	12.47 m	
Point 2	43.744 m	14.09 m	
Point 3	48.307 m	15.96 m	
Point 4	60.176 m	16.39 m	
Point 5	71.547 m	10.51 m	
Point 6	110 m	10.51 m	
Point 7	110 m	-10 m	
Point 8	0 m	-10 m	
Point 9	0 m	9.47 m	
Point 10	33.0667 m	9.47 m	
Point 11	33.96945 m	9.86061 m	
Point 12	0 m	8.39 m	
Point 13	110 m	8.39 m	

# Regions

	Material	Points	Area
Region 1	Sandy Clay	1,11,5,4,3,2	147.79 m²
Region 2	Clayey Sand	10,9,12,13,6,5,11	185.85 m²
Region 3	Sandy Clay	8,7,13,12	2,022.9 m <sup>2</sup>

# **Current Slip Surface**

Slip Surface: 83 Factor of Safety: 1.953 Volume: 49.187049 m<sup>3</sup> Weight: 959.5182 kN Resisting Moment: 9,726.6361 kN·m Activating Moment: 4,980.2654 kN·m Resisting Force: 555.45852 kN Activating Force: 284.50158 kN Slip Rank: 1 of 125 slip surfaces Exit: (76.698394, 10.51) m Entry: (56.99386, 16.274715) m Radius: 15.621786 m Center: (70.152579, 24.694234) m

	х	Y	PWP	Base Normal Stress	Frictional Strength	Cohesive Strength
Slice 1	57.312074 m	15.81456 m	0 kPa	1.5931883 kPa	0.74291589 kPa	10 kPa

Slice	57.948502	14.95563	0	15.432752	7.1964103	10 kDa
2	m	m	kPa	kPa	kPa	10 kPa
Slice 3	58.58493 m	14.205895 m	0 kPa	27.503465 kPa	12.825076 kPa	10 kPa
Slice	59.221358	13.542999	0	38.308393	17.863497	10 kPa
4	m	m	kPa	kPa	kPa	
Slice 5	59.857786 m	12.952073 m	0 kPa	48.202651 kPa	22.477265 kPa	10 kPa
Slice	60.486419	12.428454	0 kPa	54.688407	25.501623	10 kPa
6	m	m		kPa	kPa	
Slice 7	61.107258 m	11.963273 m	0 kPa	57.863793 kPa	26.98233 kPa	10 kPa
Slice	61.728096	11.543858	0	60.590893	28.253997	10 10
8	m	m	kPa	kPa	kPa	10 kPa
Slice	62.348935	11.165934	0	62.923804	29.341852	10 kPa
9	m	m	kPa	kPa	kPa	
Slice 10	62.969774 m	10.826094 m	0 kPa	64.890644 kPa	30.259004 kPa	10 kPa
Slice	63.590612	10.521592	0	66.497586	31.008334	10 kPa
11	m	m	kPa	kPa	kPa	
Slice 12	64.219614 m	10.247037 m	0 kPa	67.52588 kPa	38.986085 kPa	2 kPa
Slice	64.856778	10.001379	0	67.889748	39.196164	2 1/00
13	m	m	kPa	kPa	kPa	2 kPa
Slice	65.493942	9.7869913	0	67.817683	39.154557	2 kPa
14	m	m	kPa	kPa	kPa	
Slice	66.131106	9.6025394	0	67.241526	38.821913	2 kPa
15	m	m	kPa	kPa	kPa	2 11 0
Slice	66.76827	9.4469342	0	66.082619	38.152818	2 kPa
16	m	m	kPa	kPa	kPa	
Slice	67.405434	9.3192981	0	64.255295	37.097812	2 kPa
17	m	m	kPa	kPa	kPa	
Slice	68.042598	9.2189378	0	61.671472	35.606041	2 kPa
18	m	m	kPa	kPa	kPa	
Slice	68.679762	9.1453241	0	58.246405	33.628578	2 kPa
19	m	m	kPa	kPa	kPa	
Slice	69.316926	9.0980777	0	53.905501	31.122355	2 kPa
20	m	m	kPa	kPa	kPa	
Slice	69.95409	9.0769588	0	48.591812	28.054496	2 kPa
21	m	m	kPa	kPa	kPa	
Slice	70.591254	9.0818612	0	42.273574	24.406659	2 kPa
22	m	m	kPa	kPa	kPa	
Slice 23	71.228418	9.1128096	0 kPa	34.950865 kPa	20.178891 kPa	2 kPa
	m	m				
Slice 24	71.868962 m	9.1704041 m	0 kPa	30.424452 kPa	17.565566 kPa	2 kPa
Slice	72.512886	9.255223	0	20 02742 50-	16.649298	2 40-
25	m	m	kPa	28.83743 kPa	kPa	2 kPa
Slice	73.156811	9.3675532	0	26.429987	1E 25020 hp-	2 40-
26	m	m	kPa	kPa	15.25936 kPa	2 kPa
						1

Slice	73.800735	9.5080064	0	23.221425	13.406896	
27	m	m	kPa	kPa	kPa	
Slice	74.444659	9.6773731	0	19.256254	11.117603	2 kPa
28	m	m	kPa	kPa	kPa	
Slice	75.088584	9.8766468	0	14.600272	8.4294708	2 kPa
29	m	m	kPa	kPa	kPa	
Slice	75.732508	10.107056	0	9.3339166	5.3889393	2 kPa
30	m	m	kPa	kPa	kPa	
Slice	76.376432	10.370107	0	3.5436844	2.0459471	2 kPa
31	m	m	kPa	kPa	kPa	



# Appendix F – Photos



Photo 1



Photo 2





Photo 3



Photo 4





Photo 5



Photo 6



Geotechnical Investigation & Dam Stability Assessment Project: 1075 Horseshoe Bend Road, Torquay Client: The Dunes, Torquay Report No: AGTE17463



Photo 6



Photo 7





Photo 8



Photo 9



Geotechnical Investigation & Dam Stability Assessment Project: 1075 Horseshoe Bend Road, Torquay Client: The Dunes, Torquay Report No: AGTE17463



Photo 10



Photo 11



Geotechnical Investigation & Dam Stability Assessment Project: 1075 Horseshoe Bend Road, Torquay Client: The Dunes, Torquay Report No: AGTE17463



Photo 12



Photo 13